Appendix 27.
Fountain Head Evaporator Emissions Study

MINETEK

Technical Memorandum

To: Craig Wilson | Project Mining & Infrastructure Manager

From: Sean Edwards | Engineering Lead

Subject: **Fountain Head Evaporator Emissions Study**

I. Introduction

Minetek has been engaged to perform a particulate emissions study on a proposed evaporation system to be installed at the PNX Metals Fountain Head Gold Mine, NT. The particulate emission of interest is Arsenic PM10 and PM2.5 and is to be compared to the relevant standards.

The proposed system consists of 3 x Minetek 600/300 evaporators, a 112.5L/s pump and MCC with automation, including flow/pressure/weather monitoring, to manage and log the system parameters. The system has been proposed to be installed at the Fountain Head Pit Lake for Phase 1 and then to be moved to the evaporation dam for Phase 2 a set time after.

In addition to the particulate emission study the system setup parameters will be investigated to suggest parameters to improve the runtime and evaporation efficiency.

II. Minetek Evaporation Rate, Spray Drift & Particulate Emissions Model – T-Mine

The primary purpose of employing this method is to assess and estimate airborne particulate matter as a result of mechanically enhanced evaporation. Minetek invested many months of research and laboratory testing in 2016 to develop an internal program to estimate airborne particulate emissions with consultation with the University of Queensland who developed the USA AgDRIFT model. The modelling tool became available to Minetek for use in 2017 and is proprietary to Minetek and is not commercially available.

This modelling technique calculates the expected individual droplet volume loss, for each droplet size, at 0.1 second intervals across the full theoretical trajectory. The calculation has multiple inputs of which more accurate data entry results in a higher level of confidence in the model results. As a result of the model design it calculates evaporation rates in line with the particulate assessment.

The basis of this method is that the evaporation rate can be described as a droplet diameter change proportional to time.

Whilst the program is very large and requires multiple runs to complete a full data set, in short T-Mine performs the following steps to derive expected evaporation efficiency, spray drift and particulate emissions:

1) Data Entry – The following inputs are required as a minimum
    a. Ambient temperature (dry bulb) and relative humidity are input to calculate the wet bulb temperature. This is the theoretical limit lowest temperature achieved by adiabatic evaporation of water in the air, until the air is saturated.
    b. Windspeed
    c. Release height
    d. Solids concentration
    e. Water density
    f. Air density
    g. Evaporator details regarding nozzle type, # of nozzles and system water pressure.

2) T-Mine then generates a Gaussian distribution of droplet sizes to evaluate the expected output from the evaporator (droplet diameter vs. frequency of occurrence).

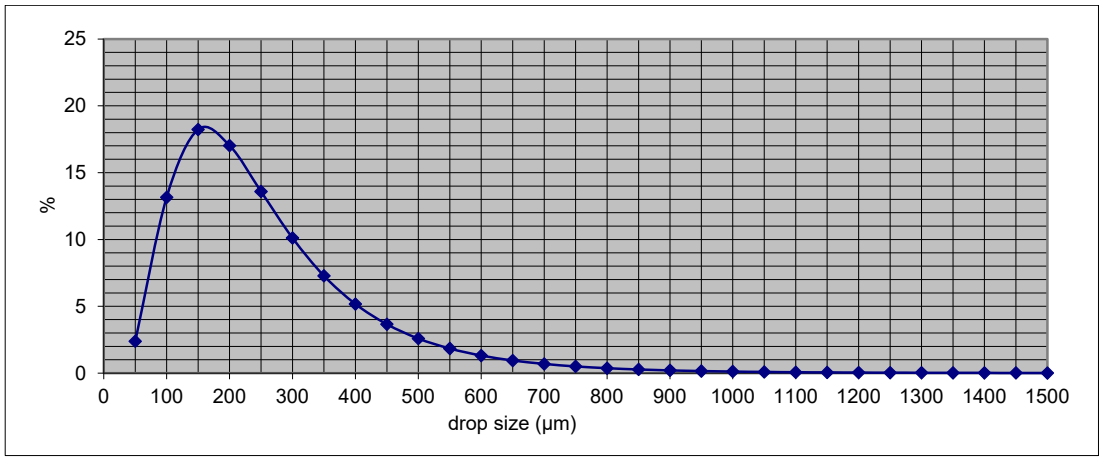


Figure 1 - Distribution showing droplet frequency by size

3) The program then employs the GDS (Gaussian Diffusion and Sedimentation) model developed with the University of Queensland and looks at the time in flight for each size particle within the overall evaporator spray plume. The model calculates the projectile trajectory through the parabolic function with standard fluid factors considered such as drag.

    These inputs are used to then run the model to calculate the change in water droplet size (µm/s) and initial vector conditions of the droplets.

4) The expected horizontal distance travelled by each droplet size is then calculated and final droplet size (using the evaporation rate in step 2 and referenced formula), with end conditions being set at either impact with pond/ground or evaporation of all liquid which will result in drift of solids.

5) The cumulative final droplet volumes are then compared against the initial volumes, making allowance for dissolved particles, to calculate overall efficiency and spray drift distance per droplet size.

6) All droplets smaller than the VMDcrit (Smallest droplet size that will hit the ground) result in particulate emissions and the volume is calculated to determine the solute production rate.

7) The cumulative density of droplets containing the PM of interest is then determined to calculate the PM of interest solute production rate

8) The concentration of the PM of interest at a set distance (x,y,z) from the source is then calculated using the gaussian dispersion model and compared to the standard to verify compliance,

III. Evaporation System Parameters

1. Weather Data

The weather data used for the purpose of this analysis is hourly temperature, humidity, wind speed and wind direction data for the period 2015 – 2019 and has been obtained from the Australian Government, Bureau of Meteorology (BoM) station 14901, Douglas River Research Farm. See appendix C.

The data has been assessed to determine the following:

- Best location and orientation of the evaporators to optimise the runtime and yearly volume evaporated
- Optimal evaporation efficiency
- Maximum allowable windspeed

Once these parameters are confirmed, the year average and peak Arsenic emissions can be calculated and compared to the relevant standards.

For this study, the minimum and maximum temperature and humidity is 0/45°C and 0/95% respectively due to equipment operating limitations and precipitation.

2. Wind Speed Considerations

Two maximum windspeeds has been considered, one ensuring containment of the unevaporated droplets to the pond, and the other ensuring containment within a 500m radius.

Being smaller in size, the Fountain Head Pit Lake and the phase 1 location has been selected for calculating the maximum allowable wind speed to ensure containment. The lake has an odd shape but 320m has been used as the average distance to the opposite shore from where the evaporators are proposed to be installed. See figure 2 for the proposed phase 1 installation location.

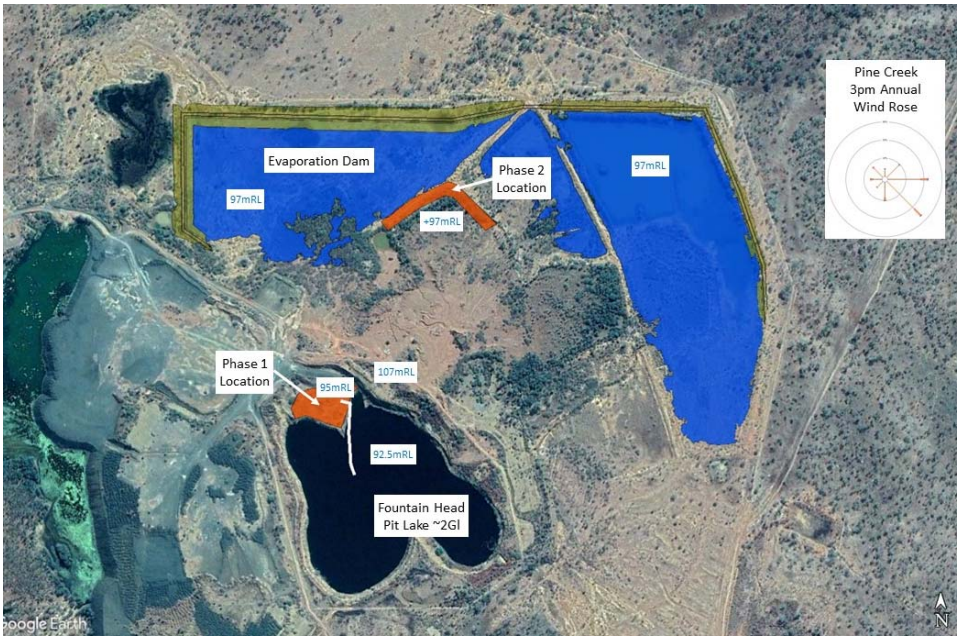


Figure 2 – Propose evaporator installation location (Image courtesy Craig Wilson – PNX Metals)

Using the T-Mine model to track the trajectory of each droplet size, the ultimate destination of each droplet size has been determined based on a worst-case temperature/humidity combination and the maximum allowable windspeed calculated. See figure 3 for a typical instantaneous view of the travel distance per droplet size. Note that droplets that do not reach 0m (hit the ground) are droplets that evaporate to dryness and thus result in particulate emissions.

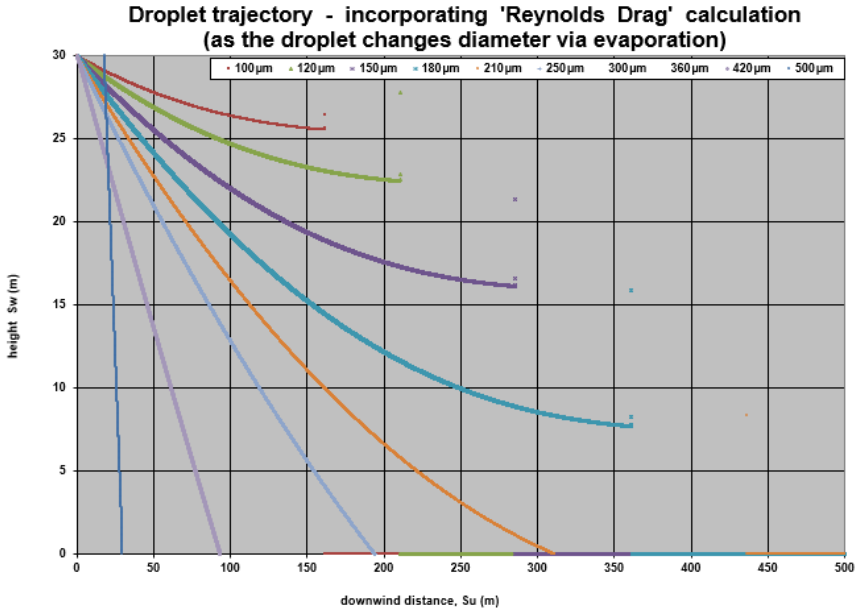


Figure 3 – Typical Droplet Trajectory

Employing this methodology, the maximum allowable windspeeds for the system while ensuring containment of the non-evaporated droplets within the 320m and 500m radii has been calculated as 6m/s and 7.6m/s respectively.

Using 7.6m/s over 6m/s results in an increase in evaporator runtime of 4% over a year of operation.

3. Wind Direction Considerations

By scrutinising the weather data, it has been found that the predominant wind direction changes based on the season and will greatly affect the evaporator runtime and thus the amount of water evaporated.

In this report the "dry season" is defined as April to August (5 months) and the "wet season" as September to March (7 months) due to the change in predominant wind direction as seen in figures 4 - 6. Note: For all weather data considered, wind speeds in excess of the maximum allowable wind speed has been disregarded as the evaporators will not be running.

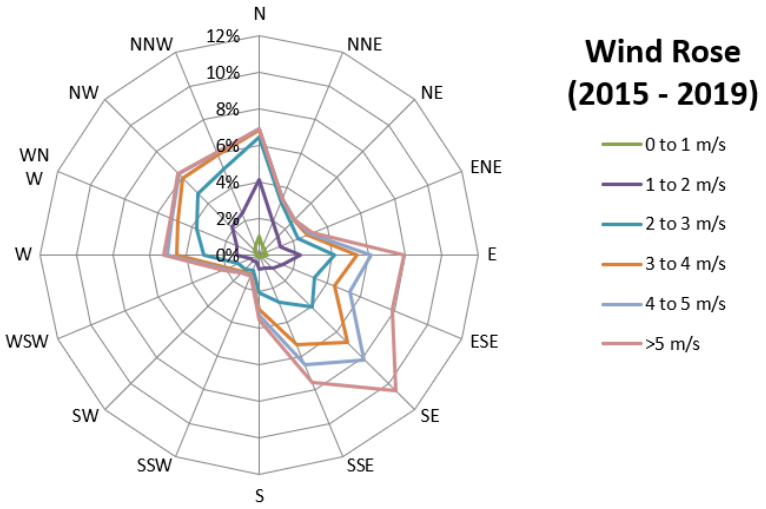


Figure 4 - All Year Wind Rose (Derived from 2015-2019 weather data received from the BoM)

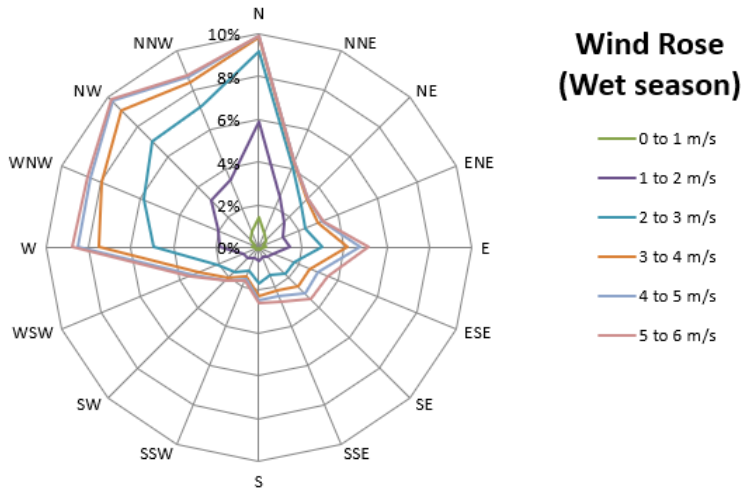


Figure 5 - Wet Season Wind Rose

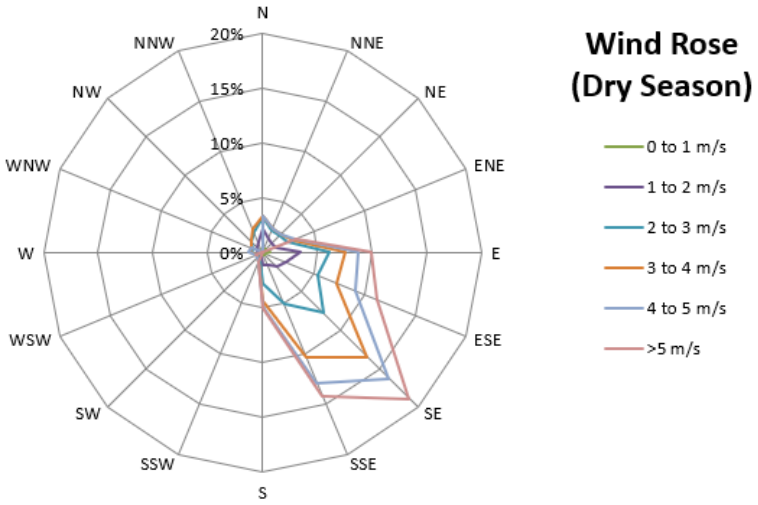


Figure 6 - Dry Season Wind Rose

Based on these findings, Minetek would propose installation of the evaporators on the North Westerly bank of the lake in the wet season, and on the South Easterly bank in the dry season, as indicated on figure 7.

Figure 7 - Proposed Phase 1 Dry/Wet season Installation Positions

Should spray drift need to be contained to the pond area, wind direction limitations can be set. The philosophy Minetek employs is a defined allowable spray arc which limits spray within two bounds as depicted in Figure 8. For the scenario where the evaporators are located North West, the limits would be defined as 50deg to 220deg and for South East 230deg to 40deg with North being 0deg.

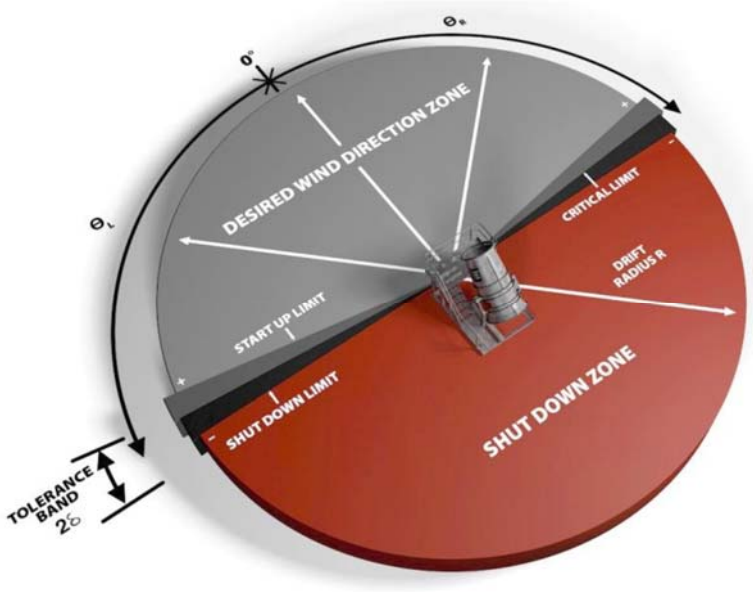


Figure 8 - Evaporator allowable spray arc

4. Operating Scenario Comparison

T-mine modelling has been performed for different scenarios based on the installation locations, maximum windspeed and wind direction limitations defined. See table 1 for a summary of the results and refer to Appendix A for monthly reports for each of the scenarios.

#	Operating location	Windspeed Limit (m/s)	Spray direction limit (°)	Evaporator Runtime (%)	Evaporator Efficiency (%)	Volume Evaporated per year (ML)
1	NW	-	-	90	39.5	1271.4
2	NW	6	-	85	39.5	1200.3
3	NW	6	50-220	47	34.6	586.9
4	SE	6	230-40	50	39	720.4
5	NW in wet season & SE in dry season	6	50-220 – NW 230-40 – SE	65	38.4	891.3
6	NW in wet season & SE in dry season	7.6	-	89	39.9	1273.4

Table 1 - Operating scenario comparison

Note: Volume evaporated per year is only the added benefit of mechanically enhanced evaporation and excludes pan evaporation.

Scenario #6 has been selected for the emissions study as it will result in the highest amount of emissions, while maintaining successful containment of non-evaporated water droplets within a 500m radius of the setup location. Operation is regardless of wind direction and measures will need to be taken to limit recirculation of droplets through the fan.

Droplets smaller than 210µm will evaporate to dryness and the percentage of droplets in comparison to the total volume is 27.7%. This is the percentage of droplets that have the potential to become emissions and more specifically, emissions of arsenic. For the simplicity of this report it is assumed that all the arsenic contained in the droplets evaporated to dryness will result in emissions regardless of the species thereof or whether it is part of an organic compound. This is seen as the worst-case scenario as in reality some of the compounds will drop to the ground and not result in drift.

IV. Particulate Emissions

Particulate emissions are caused by the drift of droplets that evaporate to dryness. In this study the drift of PM10 and PM2.5 of Arsenic is investigated. The total particulate emission is calculated from the percentage of droplets that evaporate to dryness of which all is assumed to result in drift off site.

With the evaporation runtime, efficiency and weather limitations defined, the Arsenic particulate emissions can be determined and compared to the standard limits.

1. Emission Standards and Receptors

The standards and limits that are compared to are set out in table 2.

Averaging Period	Limit (µg/m3)	Source
1h, 99.9th Percentile	0.09	New South Wales Approved Methods
1 Year	0.006	Queensland Air EPA
1 Year	0.003	Victoria Protocol for Environmental Management, Mining and Extractive Industries
8h, TWA	50	Safe Work Australia

Table 2 - Arsenic Emission Standard Limits

The limits are defined as measured at the sensitive receptors of which three have been identified:

- R1, Grove Hill Historic Hotel
- R2, Hayes Creek Caravan Park
- R3, Rural Residence

Only the concentration at the Grove Hill Historic Hotel Receptor, R1, will be considered for this analysis as it is the closest (>6000m) to the evaporator installation location and is in line with the dominant wind direction in the wet season and will thus be the worst case scenario. Figure 9 identifies the sensitive receptor locations and distance, as the crow flies, from the evaporator installation location to R1.

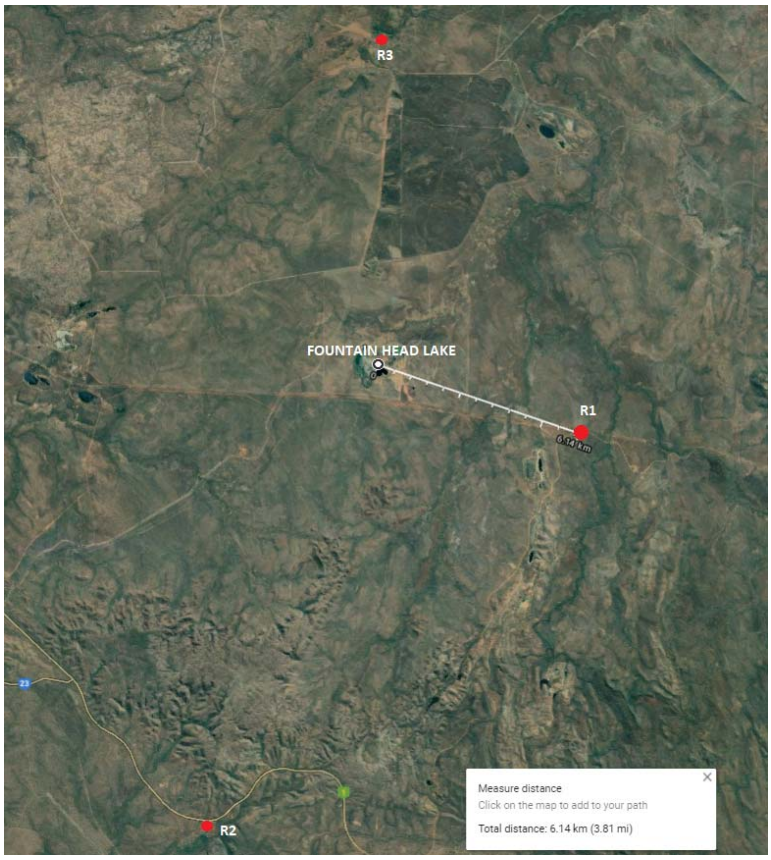


Figure 9 – Sensitive Receptor Locations

2. Analysis Parameters

Droplets evaporated to dryness are considered as particulate matter (PM) for the drift analysis and analysed using the gaussian dispersion model. The model disregards the following:

- Variable wind speed along travel path
- Complex terrain
- Spatial and temporal changes in meteorological conditions
- Deposition within plume travel time (Non-sedimenting)

For the 99.9th percentile of Arsenic analysis, the following parameters have been set to determine the solute production rate:

- Maximum windspeed used as average along travel route
- Highest evaporation rate (resulting in the highest amount of PM produced)
- Plume release height set to the peak of the evaporator spray trajectory
- 100% Evaporator Runtime
- Arsenic concentration of 784µg/L (99.9th percentile)

For the year averaged results the parameters obtained in scenario #6 and an Arsenic concentration of 526µg/L have been used.

3. Results

The particulate emissions have been determined using the T-mine model and compared to the different standard limits. Results are summarised in table 3 and calculations can be found in appendix B.

Arsenic PM Considered	Concentration (µg/m3) @ R1	Compliance Limit (µg/m3)	Compliant?
99.9th percentile water Arsenic content (784µg/L)			
PM10	0.00264	0.09 / 50	Yes
PM2.5	0.00025		Yes
Annual average Arsenic content (526µg/L)			
PM10	0.001352	0.006 / 0.003	Yes
PM2.5	0.000129		Yes

Table 3 - Particulate Emission Summary

The Arsenic concentration at R1, and thus R2 & R3, will comply to the relevant standards should the system be installed.

V. Summary

Using the T-Mine model it can be demonstrated that the arsenic emissions produced by the proposed Minetek Evaporation System can comply with the limits set out by the relevant standards as measured at the sensitive receptors. This can be achieved while running the system 24h per day and 12 months per year without excessive limits on the operation.

APPENDIX A – Evaporation Efficiency/Runtime Reports

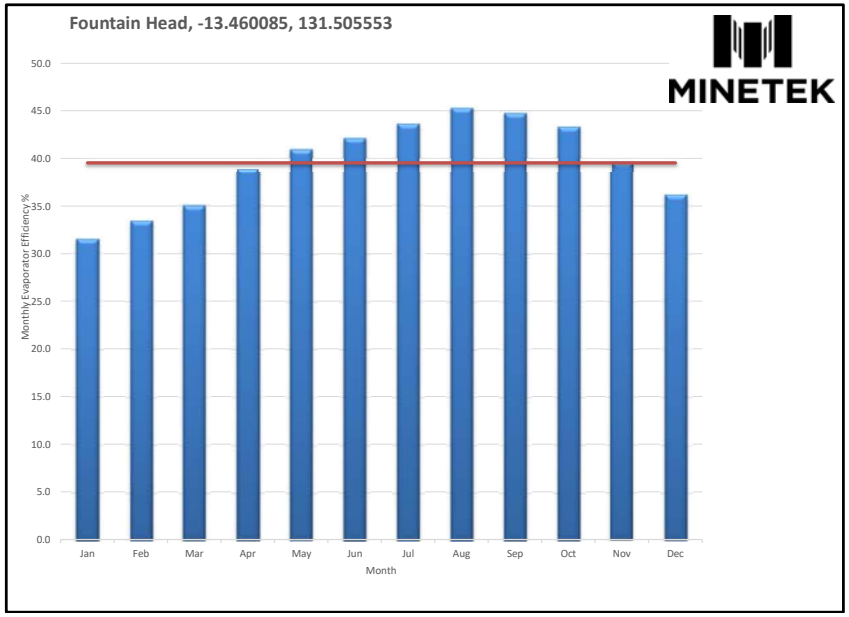
Scenario # 1

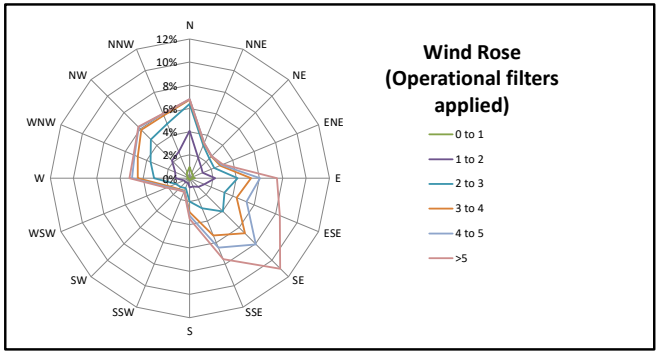
Site/Location:	PNX Metals: Fountain Head, -13.460085, 131.505553
Project Scope:	PM2.5 & PM10 Study
Weather Data Source:	http://www.bom.gov.au/climate/averages/tables/cw_014901_All.shtml
Weather Data Location:	Douglas River Research Farm

Month:	**Jan**	**Feb**	**Mar**	**Apr**	**May**	**Jun**	**Jul**	**Aug**	**Sep**	**Oct**	**Nov**	**Dec**
Average Relative Humidity (%):	79.6	77.2	74.7	66.0	58.2	55.0	51.6	48.3	53.2	59.7	67.5	73.5
Average Temperature (°C):	28.5	28.8	29.0	27.4	25.0	23.0	22.7	24.0	27.6	29.7	29.7	29.3
Average Wind Speed (m/s):	2.1	2.0	1.9	2.1	2.8	3.1	2.8	2.5	2.2	2.2	1.9	1.9
Efficiency Estimate (%):	31.5	33.4	35.0	39.0	40.9	42.1	43.5	45.3	44.8	43.3	39.6	36.1
Estimated Run Time (%):	77%	80%	80%	92%	96%	96%	97%	94%	89%	99%	92%	88%
Estimated Run Time (h/d avg):	18.5	19.2	19.2	22.0	23.1	23.1	23.2	22.6	21.2	23.7	22.1	21.0
Water Volume Evaporated (ML):	73.2	72.5	84.5	104.1	118.3	118.1	126.8	128.4	115.3	128.7	106.0	95.4

Average Evaporation Efficiency per Evaporator Unit (%):	39.5
Average Evaporation Run Time (%):	90%
Yearly Water Volume Evaporated (ML):	1271.4
Average Run Time (h/d):	21.6

Comments: Evaporation efficiency is estimated to be between 31.5% (Jan) and 45.3% (Aug) with an annual average of 39.5%.
The study includes the months January to December, operating from 12:00 AM to 11:59 PM
The study includes operation from 0 degrees to 359 degrees wind direction.
Temperature and Humidity limitations are 0-45°C and 0-95% respectively.





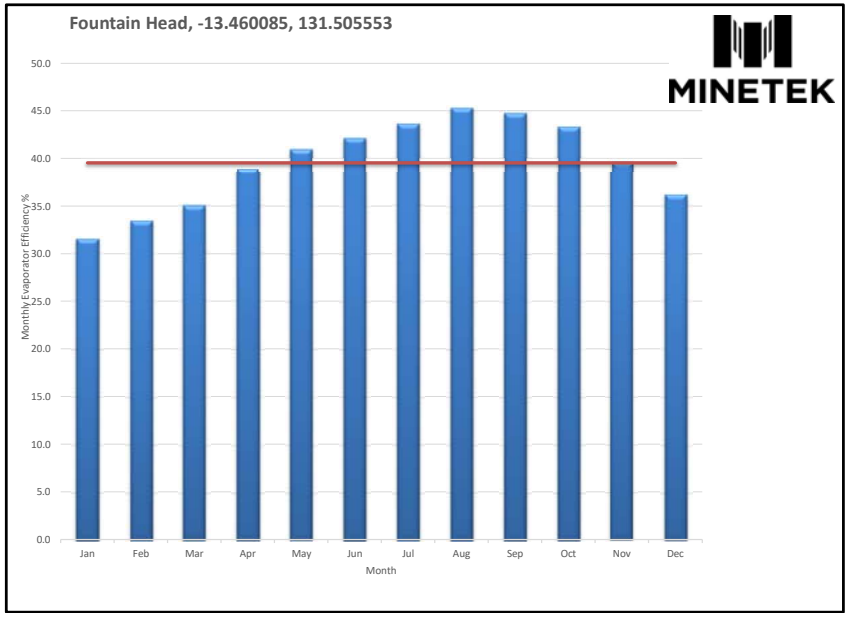
Scenario # 2

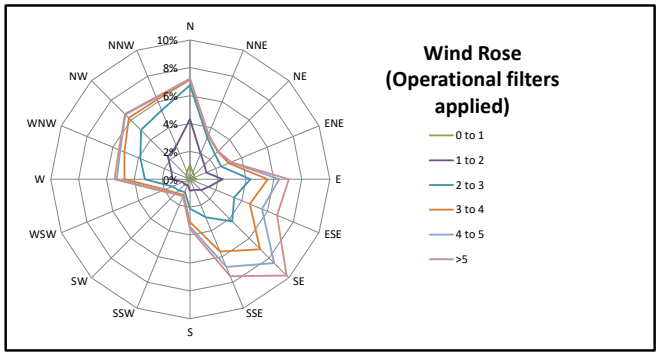
Site/Location:	PNX Metals: Fountain Head, -13.460085, 131.505553
Project Scope:	PM2.5 & PM10 Study
Weather Data Source:	http://www.bom.gov.au/climate/averages/tables/cw_014901_All.shtml
Weather Data Location:	Douglas River Research Farm

Month:	**Jan**	**Feb**	**Mar**	**Apr**	**May**	**Jun**	**Jul**	**Aug**	**Sep**	**Oct**	**Nov**	**Dec**
Average Relative Humidity (%):	79.6	77.1	75.1	67.7	62.0	57.9	54.3	50.8	55.4	60.6	67.6	73.5
Average Temperature (°C):	28.5	28.8	29.0	27.2	24.3	22.2	22.1	23.5	27.2	29.5	29.7	29.3
Average Wind Speed (m/s):	2.1	1.9	1.8	1.9	2.2	2.5	2.3	2.1	2.0	2.0	1.8	1.8
Efficiency Estimate (%):	31.5	33.4	35.0	39.0	40.9	42.1	43.5	45.3	44.8	43.3	39.6	36.1
Estimated Run Time (%):	76%	79%	78%	87%	85%	85%	87%	87%	84%	96%	91%	87%
Estimated Run Time (h/d avg):	18.3	19.0	18.8	20.9	20.5	20.4	20.9	20.9	20.1	22.9	21.8	20.9
Water Volume Evaporated (ML):	72.4	71.8	82.6	98.5	105.0	104.1	114.1	118.6	109.4	124.4	104.8	94.6

Average Evaporation Efficiency per Evaporator Unit (%):	39.5
Average Evaporation Run Time (%):	85%
Yearly Water Volume Evaporated (ML):	1200.3
Average Run Time (h/d):	20.4

Comments: Evaporation efficiency is estimated to be between 31.5% (Jan) and 45.3% (Aug) with an annual average of 39.5%.
The study includes the months January to December, operating from 12:00 AM to 11:59 PM
The study includes operation from 0 degrees to 359 degrees wind direction.
Temperature and Humidity limitations are 0-45°C and 0-95% respectively.
Maximum allowable windspeed is 6m/s





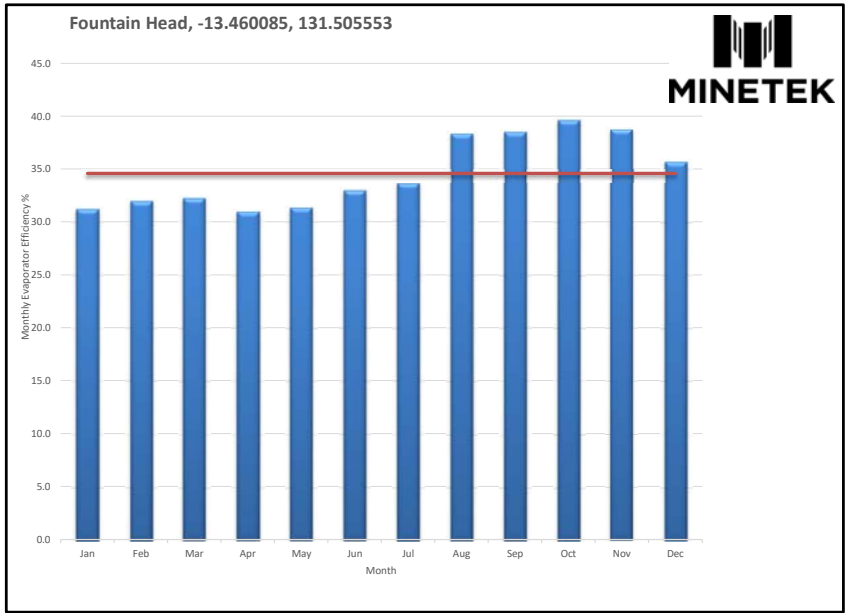
Scenario # 3

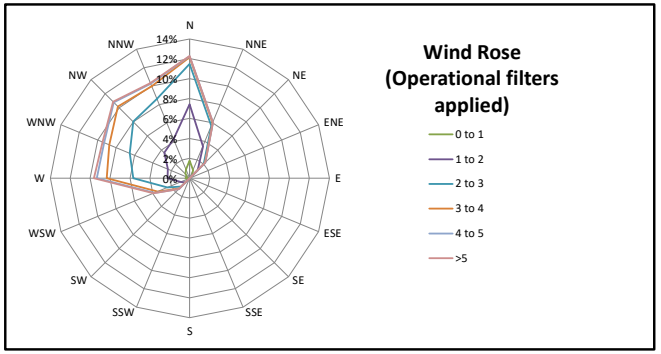
Site/Location:	PNX Metals: Fountain Head, -13.460085, 131.505553
Project Scope:	PM2.5 & PM10 Study
Weather Data Source:	http://www.bom.gov.au/climate/averages/tables/cw_014901_All.shtml
Weather Data Location:	Douglas River Research Farm

Month:	**Jan**	**Feb**	**Mar**	**Apr**	**May**	**Jun**	**Jul**	**Aug**	**Sep**	**Oct**	**Nov**	**Dec**
Average Relative Humidity (%):	79.6	78.6	78.1	79.1	77.7	74.2	72.5	65.5	67.2	66.4	68.6	73.7
Average Temperature (°C):	28.5	28.5	28.5	25.7	23.0	20.6	19.3	22.2	25.8	28.5	29.5	29.3
Average Wind Speed (m/s):	2.0	1.8	1.5	0.7	0.5	0.6	0.6	1.0	1.3	1.6	1.7	1.7
Efficiency Estimate (%):	31.2	31.9	32.2	30.9	31.3	32.9	33.6	38.3	38.5	39.6	38.7	35.7
Estimated Run Time (%):	61%	61%	51%	36%	25%	18%	25%	38%	50%	66%	68%	67%
Estimated Run Time (h/d avg):	14.6	14.7	12.2	8.7	5.9	4.4	6.1	9.1	12.1	15.9	16.3	16.2
Water Volume Evaporated (ML):	57.2	53.1	49.4	32.7	23.3	17.4	25.7	43.9	56.3	79.1	76.7	72.2

Average Evaporation Efficiency per Evaporator Unit (%):	34.6	**Yearly Water Volume Evaporated (ML):**	586.9
Average Evaporation Run Time (%):	47%	**Average Run Time (h/d):**	11.4

Comments: Evaporation efficiency is estimated to be between 30.9% (Apr) and 39.6% (Oct) with an annual average of 34.6%.
The study includes the months January to December, operating from 12:00 AM to 11:59 PM
The study includes operation from 50 degrees to 220 degrees wind direction.
Temperature and Humidity limitations are 0-45°C and 0-95% respectively.
The maximum allowed windspeed is 6m/s





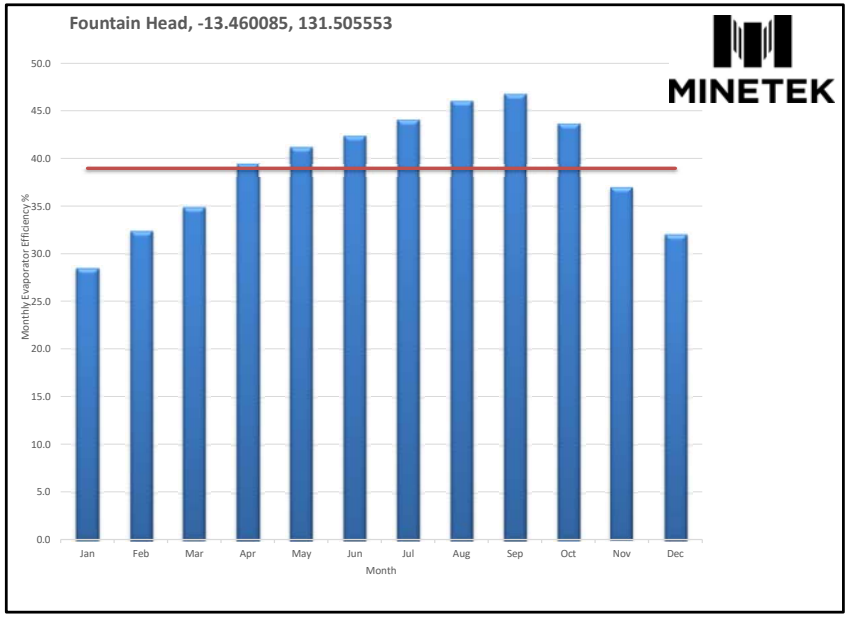
Scenario # 4

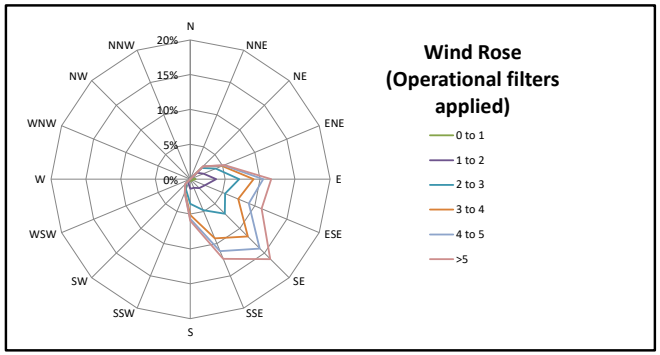
Site/Location:	PNX Metals: Fountain Head, -13.460085, 131.505553
Project Scope:	PM2.5 & PM10 Study
Weather Data Source:	http://www.bom.gov.au/climate/averages/tables/cw_014901_All.shtml
Weather Data Location:	Douglas River Research Farm

Month:	**Jan**	**Feb**	**Mar**	**Apr**	**May**	**Jun**	**Jul**	**Aug**	**Sep**	**Oct**	**Nov**	**Dec**
Average Relative Humidity (%):	82.8	77.9	74.6	66.1	60.8	56.9	52.5	47.8	49.9	58.9	71.5	78.4
Average Temperature (°C):	27.6	28.3	28.7	27.1	24.1	22.1	22.1	23.0	27.1	29.3	28.7	28.1
Average Wind Speed (m/s):	1.3	1.3	1.7	2.0	2.3	2.6	2.4	2.1	1.9	1.7	1.4	1.1
Efficiency Estimate (%):	28.4	32.4	34.8	39.4	41.1	42.3	44.0	46.0	46.7	43.7	36.9	32.0
Estimated Run Time (%):	22%	27%	39%	68%	73%	75%	75%	63%	48%	43%	34%	32%
Estimated Run Time (h/d avg):	5.4	6.6	9.3	16.4	17.5	18.0	17.9	15.2	11.5	10.4	8.3	7.6
Water Volume Evaporated (ML):	19.2	24.0	40.4	78.3	90.4	92.2	98.9	87.4	65.1	57.0	37.0	30.4

Average Evaporation Efficiency per Evaporator Unit (%):	39.0	**Yearly Water Volume Evaporated (ML):**	720.4
Average Evaporation Run Time (%):	50%	**Average Run Time (h/d):**	12.0

Comments: Evaporation efficiency is estimated to be between 28.4% (Jan) and 46.7% (Sep) with an annual average of 39%.
The study includes the months January to December, operating from 12:00 AM to 11:59 PM
The study includes operation from 230 degrees to 40 degrees wind direction.
Temperature and Humidity limitations are 0-45°C and 0-95% respectively.
The maximum allowed windspeed is 6m/s





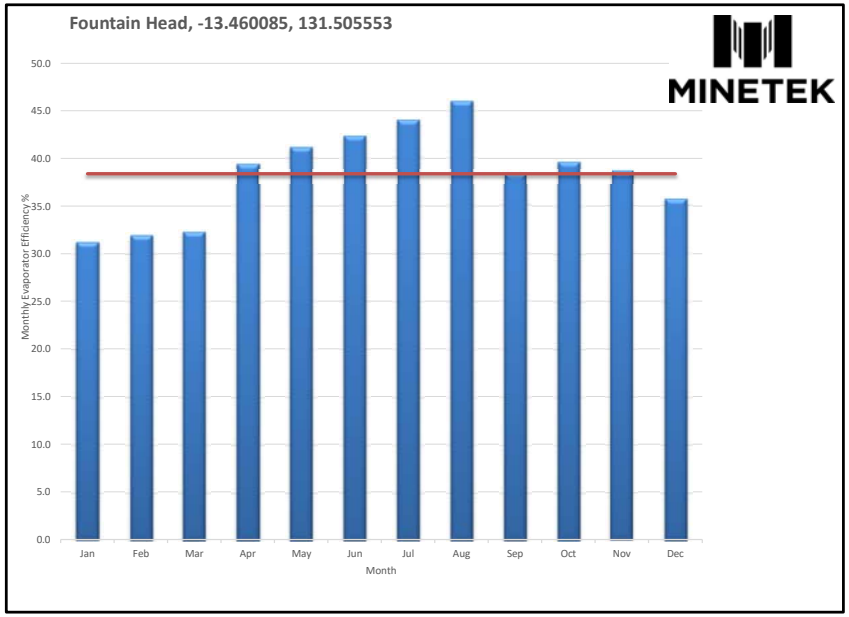
Scenario # 5

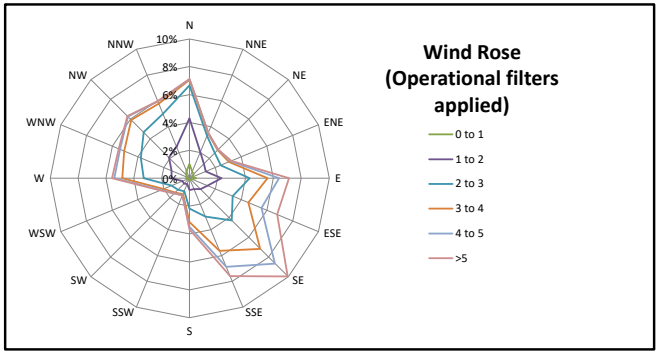
Site/Location:	PNX Metals: Fountain Head, -13.460085, 131.505553
Project Scope:	PM2.5 & PM10 Study
Weather Data Source:	http://www.bom.gov.au/climate/averages/tables/cw_014901_All.shtml
Weather Data Location:	Douglas River Research Farm

Month:	**Jan**	**Feb**	**Mar**	**Apr**	**May**	**Jun**	**Jul**	**Aug**	**Sep**	**Oct**	**Nov**	**Dec**
Average Relative Humidity (%):	79.1	76.6	74.5	67.1	61.5	57.5	53.9	50.4	54.9	60.1	67.1	73.0
Average Temperature (°C):	28.6	28.9	29.1	27.3	24.4	22.3	22.2	23.6	27.4	29.6	29.8	29.4
Average Wind Speed (m/s):	2.1	1.9	1.9	1.9	2.3	2.6	2.3	2.1	2.0	2.0	1.9	1.8
Efficiency Estimate (%):	31.2	31.9	32.2	39.4	41.1	42.3	44.0	46.0	38.5	39.6	38.7	35.7
Estimated Run Time (%):	61%	61%	51%	68%	73%	75%	75%	63%	50%	66%	68%	67%
Estimated Run Time (h/d avg):	14.6	14.7	12.2	16.4	17.5	18.0	17.9	15.2	12.1	15.9	16.3	16.2
Water Volume Evaporated (ML):	57.2	53.1	49.4	78.3	90.4	92.2	98.9	87.4	56.3	79.1	76.7	72.2

Average Evaporation Efficiency per Evaporator Unit (%):	38.4	**Yearly Water Volume Evaporated (ML):**	891.3
Average Evaporation Run Time (%):	65%	**Average Run Time (h/d):**	15.6

Comments: Evaporation efficiency is estimated to be between 31.2% (Jan) and 46% (Aug) with an annual average of 38.4%.
The study includes the months January to December, operating 24h/d
This study includes operation of the system from the NW in the wet season, and SE in the dry season
Temperature and Humidity limitations are 0-45°C and 0-95% respectively.
The maximum allowed windspeed is 6m/s





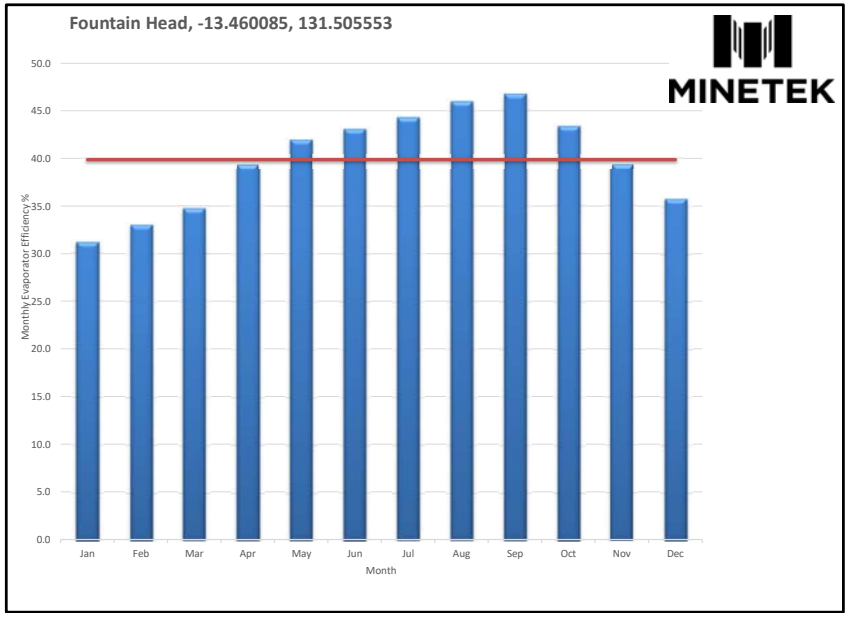
Scenario # 6

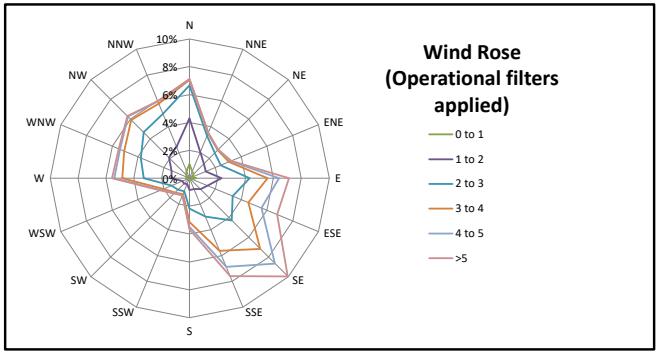
Site/Location:	PNX Metals: Fountain Head, -13.460085, 131.505553
Project Scope:	PM2.5 & PM10 Study
Weather Data Source:	http://www.bom.gov.au/climate/averages/tables/cw_014901_All.shtml
Weather Data Location:	Douglas River Research Farm

Month:	**Jan**	**Feb**	**Mar**	**Apr**	**May**	**Jun**	**Jul**	**Aug**	**Sep**	**Oct**	**Nov**	**Dec**
Average Relative Humidity (%):	79.1	76.6	74.5	67.1	61.5	57.5	53.9	50.4	54.9	60.1	67.1	73.0
Average Temperature (°C):	28.6	28.9	29.1	27.3	24.4	22.3	22.2	23.6	27.4	29.6	29.8	29.4
Average Wind Speed (m/s):	2.1	1.9	1.9	1.9	2.3	2.6	2.3	2.1	2.0	2.0	1.9	1.8
Efficiency Estimate (%):	31.1	33.0	34.7	39.3	42.0	43.1	44.3	46.0	46.7	43.3	39.4	35.8
Estimated Run Time (%):	77%	80%	79%	91%	92%	93%	94%	93%	94%	98%	92%	87%
Estimated Run Time (h/d avg):	18.5	19.2	19.0	21.8	22.1	22.3	22.6	22.3	22.6	23.5	22.1	20.9
Water Volume Evaporated (ML):	72.2	71.5	83.1	103.8	116.3	117.2	125.7	129.1	127.3	128.0	105.3	94.1

Average Evaporation Efficiency per Evaporator Unit (%):	39.9
Average Evaporation Run Time (%):	89%
Yearly Water Volume Evaporated (ML):	1273.4
Average Run Time (h/d):	21.4

Comments: Evaporation efficiency is estimated to be between 31.1% (Jan) and 46.7% (Sep) with an annual average of 39.9%.
The study includes the months January to December, operating 24h/d
This study includes operation of the system from the NW in the wet season and SE in the dry season, operating regardless of wind direction.
Temperature and Humidity limitations are 0-45°C and 0-95% respectively.
The maximum allowed windspeed is 7.6m/s





APPENDIX B – Particulate Emission Reports

MINETEK

Site/Location:	PNX Metals: Fountain Head, -13.460085, 131.505553
Scope:	99.9th Percentile Arsenic Emissions
Weather Data Source:	http://www.bom.gov.au/climate/averages/tables/cw_014901_All.shtml
Weather Data Location:	Douglas River Research Farm

Operational Parameters & Limits				**Notes**
Evaporator Type			600/300	
No of Units		ul	3	
Volume flowrate per evaporator	Q	L/s	37.4	Minetek Evaporator model volume flow rate
Effective amount evaporated	η		46.7%	Peak Minetek Evaporator Efficiency
Evaporator "Runtime"			100%	Runtime Considered For TWA
Months of Operation per Year		mo/yr	12	Operating months
Hours of Operation per Day		hr/d	24	Operating hours
Allowable spray direction: Start-End		°	(Variable)	Specified limitations on spray direction
Temperature Range: Min-Max		°C	0-45	Operational Temperature Limits
Humidity Range: Min-Max		%	0-95	Operational Humidity Limits
Plume Properties				
Maximum Plume Height	h	m	22.5	Minetek Evaporator Plume Height
Initial conc invol. (ppm)		ppm	0.784	99.9th Percentile Arsenic per client supplied water quality data
Solute Density	ρ	kg/m3	1.00	Client specified solute density
Droplet size relative to PM size	D'	x PM size	15.98	= (1/(PPM/10^6))^(1/3)
Initial conc invol. (mg/L)		mg/L	0.00078	= TDS x Solute Density
Total solute production rate	e	g/s	0.04115	= Flowrate x Concentration (mg/L) x Runtime x Evaporation Efficiency x No. of Units
Droplet size associated with PM of concern				
PM		µm	10	Client defined PM of interest
Droplet Size that contain PM of concern		µm	159.81	= PM x D'
Cumulative density (%)	Cd	%	23.05	Based on weather data and Minetek evaporator spray droplet size distribution, this is the percentage that will result in drift
PM10 emission rate	E1	g/s	0.009483	= e x cumulative density / CF
		kg/yr	299.063	
Suppression Factor			90%	Considers suppression offered by non-evaporated droplets
PM10 emission rate - suppressed	E2	kg/yr	29.91	= E1 x Supression Factor
PM10 drift rate - suppressed, Arsenic		%	2.30	= E2 / e (t/yr)

PM = size of particulate matter produced
Droplet = the size of the droplet that will produce that PM
VMDcrit = The droplet size that will hit the ground (i.e. not result in drift).
Cd = Percentage of droplets that will result in drift
E1 = Non-suppressed emission rate
E2 = Suppressed emission rate

PM (µm)	Droplet (µm)	Cd	E1 (kg/yr)	E2 (kg/yr)
2.5	39.95	2.19	28.427	2.843
10	159.81	23.05	299.063	29.906
25	399.53	73.70	956.306	95.631
Droplet size that reached the ground (VMDcrit) = 210µm				

PM10 emission concentration @ x,y,z			
Axial measurement distance	x	6000	m
Lateral distance off plume	y	0	m
Distance off ground	z	0	m
PM origin height	h	22.5	m
Avg wind speed enroute	u	6.00	m/s
PM10 emission rate - Arsenic		0.000948	g/s
Pascalli Stability Category		E	
Gausian distribution factors	a	Use tables	
	b	Use tables	
	c	6.25	
	d	0.54287	
Deviation angle	Θ	0.092	
Std. deviation y	σy	257.8	m
Std. deviation z	σz	70.0	m
PM10 Concentration @ x,y,z	C(x,y,z)	0.00264782	µg/m3

PM2.5 emission concentration @ x,y,z			
Axial measurement distance	x	6000	m
Lateral distance off plume	y	0	m
Distance off ground	z	0	m
PM origin height	h	22.5	m
Avg wind speed enroute	u	6.00	m/s
PM2.5 emission rate - Arsenic		0.0000901	g/s
Pascalli Stability Category		E	
Gausian distribution factors	a	Use tables	
	b	Use tables	
	c	6.25	
	d	0.54287	
Deviation angle	Θ	0.092	
Std. deviation y	σy	257.8	m
Std. deviation z	σz	70.0	m
PM2.5 Concentration @ x,y,z	C(x,y,z)	0.00025169	µg/m3

MINETEK

Site/Location:	PNX Metals: Fountain Head, -13.460085, 131.505553
Project Scope:	Year Average Arsenic Emissions
Weather Data Source:	http://www.bom.gov.au/climate/averages/tables/cw_014901_All.shtml
Weather Data Location:	Douglas River Research Farm

Operational Parameters & Limits				**Notes**
Evaporator Type			600/300	
No of Units		ul	3	
Volume flowrate per evaporator	Q	L/s	37.4	Minetek Evaporator model volume flow rate
Effective amount evaporated	η		39.9%	Year Average Evaporation Efficiency
Yearly Evaporator "Runtime"			89%	Year Average Runtime
Months of Operation per Year		mo/yr	12	Operating months
Hours of Operation per Day		hr/d	24	Operating hours
Allowable spray direction: Start-End		°	(Variable)	Specified limitations on spray direction
Temperature Range: Min-Max		°C	0-45	Operational Temperature Limits
Humidity Range: Min-Max		%	0-95	Operational Humidity Limits
Plume Properties				
Maximum Plume Height	h	m	22.5	Minetek Evaporator Plume Height
Initial conc invol. (ppm)		ppm	0.526	Annual Average Arsenic per client supplied water quality data
Solute Density	ρ	kg/m3	1.00	Client specified solute density
Droplet size relative to PM size	D'	x PM size	15.98	= (1/(PPM/10^6))^(1/3)
Initial conc invol. (mg/L)		mg/L	0.00053	= TDS x Solute Density
Total solute production rate	e	g/s	0.02102	= Flowrate x Concentration (mg/L) x Runtime x Evaporation Efficiency x No. of Units
Droplet size associated with PM of concern				
PM		µm	10	Client defined PM of interest
Droplet Size that contain PM of concern		µm	159.81	= PM x D'
Cumulative density (%)	Cd	%	23.05	Based on weather data and Minetek evaporator spray droplet size distribution, this is the percentage that will result in drift
PM10 emission rate	E1	g/s	0.004844	= e x cumulative density / CF
		kg/yr	152.751	
Suppression Factor			90%	Considers suppression offered by non-evaporated droplets
PM10 emission rate - suppressed	E2	kg/yr	15.28	= E1 x Supression Factor
PM10 drift rate - suppressed, Arsenic		%	2.3048	= E2 / e (t/yr)

PM = size of particulate matter produced
Droplet = the size of the droplet that will produce that PM
VMDcrit = The droplet size that will hit the ground (i.e. not result in drift).
Cd = Percentage of droplets that will result in drift
E1 = Non-suppressed emission rate
E2 = Suppressed emission rate

PM (µm)	Droplet (µm)	Cd	E1 (kg/yr)	E2 (kg/yr)
2.5	39.95	2.19	14.520	1.452
10	159.81	23.05	152.751	15.275
25	399.53	73.70	488.449	48.845
Droplet size that reached the ground (VMDcrit) = 210µm				

PM10 emission concentration @ x,y,z			
Axial measurement distance	x	6000	m
Lateral distance off plume	y	0	m
Distance off ground	z	0	m
PM origin height	h	22.5	m
Avg wind speed enroute	u	6.00	m/s
PM10 emission rate - Arsenic		0.000484	g/s
Pascalli Stability Category		E	
Gausian distribution factors	a	Use tables	
	b	Use tables	
	c	6.25	
	d	0.54287	
Deviation angle	Θ	0.092	
Std. deviation y	σy	257.8	m
Std. deviation z	σz	70.0	m
PM10 Concentration @ x,y,z	C(x,y,z)	0.001352	µg/m3

PM2.5 emission concentration @ x,y,z			
Axial measurement distance	x	6000	m
Lateral distance off plume	y	0	m
Distance off ground	z	0	m
PM origin height	h	22.5	m
Avg wind speed enroute	u	6.00	m/s
PM2.5 emission rate - Arsenic		0.0000460	g/s
Pascalli Stability Category		E	
Gausian distribution factors	a	Use tables	
	b	Use tables	
	c	6.25	
	d	0.54287	
Deviation angle	Θ	0.092	
Std. deviation y	σy	257.8	m
Std. deviation z	σz	70.0	m
PM2.5 Concentration @ x,y,z	C(x,y,z)	0.0001286	µg/m3

APPENDIX C – Weather data

YYYY	MM	DD	HH24	Air Temperature in degrees C	Relative humidity in percentage %	Wind speed in km/h	Wind direction in degrees true
2015	1	1	0.0417	25.2	98	5.4	90
2015	1	1	0.0833	25	98	7.6	110
2015	1	1	0.1250	24.7	98	9.4	110
2015	1	1	0.1667	24.7	98	7.6	120
2015	1	1	0.2083	24.8	96	7.6	120
2015	1	1	0.2500	24.7	96	5.4	110
2015	1	1	0.2917	24.7	96	0	0
2015	1	1	0.3333	25.1	96	1.8	60
2015	1	1	0.3750	25	98	0	0
2015	1	1	0.4167	25.1	96	0	0
2015	1	1	0.4583	25.4	95	3.6	350
2015	1	1	0.5000	26	92	0	0
2015	1	1	0.5417	26.6	89	3.6	340
2015	1	1	0.5833	27.2	88	5.4	50
2015	1	1	0.6250	26.4	93	7.6	30
2015	1	1	0.6667	26.8	88	3.6	10
2015	1	1	0.7083	26.5	89	0	0
2015	1	1	0.7500	27	85	3.6	50
2015	1	1	0.7917	26.8	87	1.8	40
2015	1	1	0.8333	26	89	1.8	30
2015	1	1	0.8750	25.2	94	0	0
2015	1	1	0.9167	24.9	95	0	0
2015	1	1	0.9583	25	96	0	0
2015	1	1	1.0000	24.8	96	0	0
2015	1	2	0.0417	24.6	98	0	0
2015	1	2	0.0833	24.6	98	0	0
2015	1	2	0.1250	24.8	96	0	0
2015	1	2	0.1667	24.6	98	0	0
2015	1	2	0.2083	24.4	98	0	0
2015	1	2	0.2500	24.3	98	3.6	30
2015	1	2	0.2917	24	98	0	0
2015	1	2	0.3333	23.9	96	3.6	10
2015	1	2	0.3750	24.2	96	0	0
2015	1	2	0.4167	25.4	93	1.8	20
2015	1	2	0.4583	27.5	83	3.6	10
2015	1	2	0.5000	28.9	79	7.6	10
2015	1	2	0.5417	30.6	69	7.6	10
2015	1	2	0.5833	30.4	69	9.4	330
2015	1	2	0.6250	25.9	91	11.2	350
2015	1	2	0.6667	28.6	82	5.4	40
2015	1	2	0.7083	29.3	78	3.6	10
2015	1	2	0.7500	27.8	88	3.6	330
2015	1	2	0.7917	25.1	96	0	0
2015	1	2	0.8333	25.2	96	0	0
2015	1	2	0.8750	24.8	96	1.8	40
2015	1	2	0.9167	24.7	96	1.8	30
2015	1	2	0.9583	24.7	96	0	0
2015	1	2	1.0000	24.7	96	1.8	30
2015	1	3	0.0417	24.8	96	0	0
2015	1	3	0.0833	25	96	1.8	10
2015	1	3	0.1250	24.9	96	0	0
2015	1	3	0.1667	25	96	0	0
2015	1	3	0.2083	24.9	98	0	0
2015	1	3	0.2500	24.9	98	0	0
2015	1	3	0.2917	24.8	98	7.6	270
2015	1	3	0.3333	24.7	98	0	0
2015	1	3	0.3750	24.9	98	0	0
2015	1	3	0.4167	25.5	96	1.8	70
2015	1	3	0.4583	26.6	94	3.6	60
2015	1	3	0.5000	27.6	90	1.8	50
2015	1	3	0.5417	25.3	96	1.8	290
2015	1	3	0.5833	27.1	91	0	0
2015	1	3	0.6250	26.7	95	3.6	10
2015	1	3	0.6667	27.1	90	5.4	330
2015	1	3	0.7083	27.1	88	9.4	310
2015	1	3	0.7500	27.2	87	5.4	320
2015	1	3	0.7917	26.8	86	1.8	340
2015	1	3	0.8333	26.2	88	3.6	340
2015	1	3	0.8750	25.5	89	1.8	360
2015	1	3	0.9167	24.9	91	0	0
2015	1	3	0.9583	24.4	95	0	0
2015	1	3	1.0000	24.3	96	0	0
2015	1	4	0.0417	24.2	96	0	0
2015	1	4	0.0833	23.9	96	3.6	40
2015	1	4	0.1250	23.9	98	3.6	40
2015	1	4	0.1667	24.4	96	1.8	20
2015	1	4	0.2083	24.4	98	0	0
2015	1	4	0.2500	24.3	98	0	0
2015	1	4	0.2917	24.3	98	5.4	40
2015	1	4	0.3333	24.3	98	1.8	200
2015	1	4	0.3750	24.5	98	0	0
2015	1	4	0.4167	24.8	98	0	0
2015	1	4	0.4583	25.3	98	0	0
2015	1	4	0.5000	26.9	94	3.6	30
2015	1	4	0.5417	27.2	90	1.8	10
2015	1	4	0.5833	28.5	82	5.4	10
2015	1	4	0.6250	28.4	81	3.6	350
2015	1	4	0.6667	28.4	81	5.4	10
2015	1	4	0.7083	28.7	80	5.4	360
2015	1	4	0.7500	28.3	85	3.6	360
2015	1	4	0.7917	28	79	7.6	360
2015	1	4	0.8333	27.3	86	3.6	360
2015	1	4	0.8750	26.5	91	0	0
2015	1	4	0.9167	26.2	90	3.6	10
2015	1	4	0.9583	25.9	93	0	0
2015	1	4	1.0000	25.7	93	0	0
2015	1	5	0.0417	25.5	95	0	0
2015	1	5	0.0833	25.4	96	0	0
2015	1	5	0.1250	25.4	96	0	0
2015	1	5	0.1667	25.4	96	0	0
2015	1	5	0.2083	25.2	96	0	0
2015	1	5	0.2500	25.2	96	0	0
2015	1	5	0.2917	25.3	96	0	0
2015	1	5	0.3333	25.7	96	0	0
2015	1	5	0.3750	26.7	89	5.4	10
2015	1	5	0.4167	26.1	88	7.6	340
2015	1	5	0.4583	27.1	81	9.4	300
2015	1	5	0.5000	27.5	81	13	320
2015	1	5	0.5417	26.6	89	9.4	310
2015	1	5	0.5833	27.9	74	14.8	290
2015	1	5	0.6250	29.1	76	9.4	310
2015	1	5	0.6667	29	76	11.2	290
2015	1	5	0.7083	29.1	76	5.4	310
2015	1	5	0.7500	28.6	76	7.6	330
2015	1	5	0.7917	28.5	79	5.4	320
2015	1	5	0.8333	27.7	86	0	0
2015	1	5	0.8750	27.2	90	0	0
2015	1	5	0.9167	26.6	92	7.6	320
2015	1	5	0.9583	26.4	94	0	0
2015	1	5	1.0000	26.2	96	0	0
2015	1	6	0.0417	26	97	0	0
2015	1	6	0.0833	25.8	98	1.8	150
2015	1	6	0.1250	25.8	97	0	0
2015	1	6	0.1667	25.7	98	0	0
2015	1	6	0.2083	25.6	98	0	0
2015	1	6	0.2500	25.4	96	0	0
2015	1	6	0.2917	25	98	1.8	30
2015	1	6	0.3333	25.3	98	1.8	60
2015	1	6	0.3750	26.9	92	1.8	10
2015	1	6	0.4167	29	80	7.6	360
2015	1	6	0.4583	30	74	5.4	350
2015	1	6	0.5000	31.5	71	7.6	360
2015	1	6	0.5417	30.1	70	7.6	330
2015	1	6	0.5833	26.2	85	16.6	320
2015	1	6	0.6250	29.9	65	9.4	340
2015	1	6	0.6667	30.2	68	7.6	20
2015	1	6	0.7083	30.7	66	13	320
2015	1	6	0.7500	31.2	64	11.2	330
2015	1	6	0.7917	30.3	67	11.2	320
2015	1	6	0.8333	27	78	13	290
2015	1	6	0.8750	26	89	1.8	340
2015	1	6	0.9167	25.9	90	0	0
2015	1	6	0.9583	25.4	96	0	0
2015	1	6	1.0000	25.7	96	0	0
2015	1	7	0.0417	25.9	97	0	0
2015	1	7	0.0833	25.9	97	0	0
2015	1	7	0.1250	25.8	95	0	0
2015	1	7	0.1667	25.5	95	0	0
2015	1	7	0.2083	25.3	95	0	0
2015	1	7	0.2500	25.3	95	0	0
2015	1	7	0.2917	25	96	0	0
2015	1	7	0.3333	25.4	96	0	0
2015	1	7	0.3750	27.6	90	5.4	20
2015	1	7	0.4167	29.5	81	7.6	350
2015	1	7	0.4583	25	93	9.4	320
2015	1	7	0.5000	26.5	89	3.6	360
2015	1	7	0.5417	29	79	9.4	310
2015	1	7	0.5833	31	70	11.2	310
2015	1	7	0.6250	25.5	92	24.1	270
2015	1	7	0.6667	26.4	89	13	290
2015	1	7	0.7083	26.6	93	5.4	310
2015	1	7	0.7500	26.4	92	1.8	10
2015	1	7	0.7917	26.4	92	0	0
2015	1	7	0.8333	26.1	94	0	0
2015	1	7	0.8750	25.8	96	0	0
2015	1	7	0.9167	25.6	96	5.4	120
2015	1	7	0.9583	25.9	94	0	0
2015	1	7	1.0000	25.7	96	0	0
2015	1	8	0.0417	24.8	94	13	300
2015	1	8	0.0833	24.7	96	3.6	340
2015	1	8	0.1250	24.7	96	0	0
2015	1	8	0.1667	24.8	96	0	0
2015	1	8	0.2083	24.8	98	0	0
2015	1	8	0.2500	24.9	98	0	0
2015	1	8	0.2917	24.9	98	0	0
2015	1	8	0.3333	25.1	98	0	0
2015	1	8	0.3750	26.6	94	1.8	350
2015	1	8	0.4167	28.1	84	9.4	300
2015	1	8	0.4583	29	79	11.2	310
2015	1	8	0.5000	30	72	13	320

YYYY	MM	DD	HH24	Air Temperature in degrees C	Relative humidity in percentage %	Wind speed in km/h	Wind direction in degrees true
2016	1	1	0.0417	26	93	3.6	30
2016	1	1	0.0833	25.5	95	1.8	350
2016	1	1	0.1250	25.6	94	7.6	330
2016	1	1	0.1667	25.8	93	1.8	340
2016	1	1	0.2083	25.5	95	1.8	310
2016	1	1	0.2500	25.3	96	1.8	310
2016	1	1	0.2917	25.3	96	1.8	330
2016	1	1	0.3333	25.9	96	1.8	360
2016	1	1	0.3750	27.1	91	5.4	340
2016	1	1	0.4167	28.3	85	9.4	310
2016	1	1	0.4583	29.7	76	13	290
2016	1	1	0.5000	31.3	74	11.2	310
2016	1	1	0.5417	30.2	76	22.3	250
2016	1	1	0.5833	32.6	66	16.6	280
2016	1	1	0.6250	32.8	64	18.4	290
2016	1	1	0.6667	33.2	63	13	300
2016	1	1	0.7083	32.5	64	13	310
2016	1	1	0.7500	32.5	64	14.8	300
2016	1	1	0.7917	30.6	70	13	290
2016	1	1	0.8333	29.4	75	11.2	300
2016	1	1	0.8750	28.3	79	9.4	290
2016	1	1	0.9167	27.6	83	9.4	290
2016	1	1	0.9583	27.1	87	9.4	290
2016	1	1	1.0000	26.6	91	7.6	310
2016	1	2	0.0417	26.2	93	5.4	310
2016	1	2	0.0833	25.9	94	3.6	320
2016	1	2	0.1250	25.8	95	5.4	310
2016	1	2	0.1667	25.8	95	5.4	310
2016	1	2	0.2083	25.9	96	5.4	310
2016	1	2	0.2500	25.8	96	5.4	300
2016	1	2	0.2917	25.7	96	0	0
2016	1	2	0.3333	25.6	98	0	0
2016	1	2	0.3750	27.3	91	5.4	280
2016	1	2	0.4167	29.3	82	11.2	270
2016	1	2	0.4583	31.2	74	11.2	280
2016	1	2	0.5000	33.1	68	14.8	260
2016	1	2	0.5417	33.8	62	14.8	240
2016	1	2	0.5833	34.3	60	14.8	260
2016	1	2	0.6250	35.3	60	13	240
2016	1	2	0.6667	35.5	56	13	270
2016	1	2	0.7083	35.4	60	13	280
2016	1	2	0.7500	34	66	14.8	290
2016	1	2	0.7917	32.9	67	14.8	290
2016	1	2	0.8333	30.7	74	14.8	280
2016	1	2	0.8750	29.2	80	11.2	290
2016	1	2	0.9167	28.3	84	9.4	290
2016	1	2	0.9583	27.5	89	7.6	300
2016	1	2	1.0000	27.2	90	5.4	320
2016	1	3	0.0417	26.7	94	5.4	320
2016	1	3	0.0833	26.7	94	3.6	300
2016	1	3	0.1250	26.6	94	5.4	310
2016	1	3	0.1667	26.4	95	3.6	300
2016	1	3	0.2083	26	96	0	0
2016	1	3	0.2500	25.6	98	0	0
2016	1	3	0.2917	25.7	98	0	0
2016	1	3	0.3333	26.1	97	0	0
2016	1	3	0.3750	27.6	94	7.6	140
2016	1	3	0.4167	29.8	77	7.6	220
2016	1	3	0.4583	31.6	71	5.4	220
2016	1	3	0.5000	32.4	61	9.4	190
2016	1	3	0.5417	33.2	58	5.4	40
2016	1	3	0.5833	34.1	57	7.6	320
2016	1	3	0.6250	34.8	49	5.4	80
2016	1	3	0.6667	35.9	43	11.2	200
2016	1	3	0.7083	35.7	40	5.4	230
2016	1	3	0.7500	36	41	7.6	180
2016	1	3	0.7917	35.6	43	7.6	190
2016	1	3	0.8333	32.6	57	0	0
2016	1	3	0.8750	30	67	0	0
2016	1	3	0.9167	29	85	9.4	290
2016	1	3	0.9583	27.6	84	5.4	310
2016	1	3	1.0000	26.9	90	5.4	320
2016	1	4	0.0417	26.5	94	3.6	350
2016	1	4	0.0833	26.6	94	1.8	320
2016	1	4	0.1250	26.4	95	3.6	310
2016	1	4	0.1667	26.3	97	1.8	330
2016	1	4	0.2083	26.3	96	1.8	350
2016	1	4	0.2500	26.4	96	0	0
2016	1	4	0.2917	26.6	96	0	0
2016	1	4	0.3333	26.9	95	0	0
2016	1	4	0.3750	28	90	3.6	320
2016	1	4	0.4167	29.4	82	9.4	300
2016	1	4	0.4583	31.2	72	9.4	300
2016	1	4	0.5000	31.7	69	3.6	10
2016	1	4	0.5417	32.6	59	7.6	310
2016	1	4	0.5833	34.3	55	5.4	330
2016	1	4	0.6250	34.6	52	5.4	350
2016	1	4	0.6667	34.8	46	7.6	300
2016	1	4	0.7083	31.7	65	14.8	250
2016	1	4	0.7500	32.5	60	13	290
2016	1	4	0.7917	32.8	61	9.4	310
2016	1	4	0.8333	30.6	78	0	0
2016	1	4	0.8750	29.6	82	5.4	320
2016	1	4	0.9167	28.6	86	7.6	290
2016	1	4	0.9583	27.9	88	5.4	320
2016	1	4	1.0000	27.3	90	7.6	310
2016	1	5	0.0417	26.6	94	5.4	310
2016	1	5	0.0833	26.3	95	7.6	300
2016	1	5	0.1250	26.1	96	7.6	300
2016	1	5	0.1667	25.9	96	5.4	320
2016	1	5	0.2083	25.7	96	1.8	290
2016	1	5	0.2500	25.4	98	3.6	310
2016	1	5	0.2917	25.3	98	1.8	340
2016	1	5	0.3333	25.5	96	3.6	360
2016	1	5	0.3750	27.5	90	3.6	330
2016	1	5	0.4167	29.1	81	11.2	280
2016	1	5	0.4583	30.2	76	11.2	290
2016	1	5	0.5000	31.7	68	11.2	300
2016	1	5	0.5417	32.2	66	11.2	300
2016	1	5	0.5833	33.4	61	13	280
2016	1	5	0.6250	33.6	57	13	260
2016	1	5	0.6667	34.5	54	11.2	290
2016	1	5	0.7083	35	54	7.6	310
2016	1	5	0.7500	34.8	51	9.4	310
2016	1	5	0.7917	34.6	55	5.4	310
2016	1	5	0.8333	32.6	63	7.6	300
2016	1	5	0.8750	30.3	75	7.6	290
2016	1	5	0.9167	28.8	84	5.4	290
2016	1	5	0.9583	28	87	9.4	270
2016	1	5	1.0000	27.3	90	9.4	270
2016	1	6	0.0417	26.8	91	7.6	300
2016	1	6	0.0833	26.3	94	3.6	330
2016	1	6	0.1250	26	96	5.4	310
2016	1	6	0.1667	25.6	96	0	0
2016	1	6	0.2083	25.4	98	0	0
2016	1	6	0.2500	25	98	0	0
2016	1	6	0.2917	25.4	98	0	0
2016	1	6	0.3333	25.6	96	0	0
2016	1	6	0.3750	27.2	93	1.8	350
2016	1	6	0.4167	28.7	85	9.4	280
2016	1	6	0.4583	30.4	73	5.4	290
2016	1	6	0.5000	31.5	70	7.6	290
2016	1	6	0.5417	32.3	67	9.4	300
2016	1	6	0.5833	33.8	59	9.4	310
2016	1	6	0.6250	34	51	11.2	300
2016	1	6	0.6667	34.7	50	11.2	310
2016	1	6	0.7083	35	50	11.2	310
2016	1	6	0.7500	34.6	56	9.4	310
2016	1	6	0.7917	33.9	58	13	290
2016	1	6	0.8333	32.2	67	9.4	290
2016	1	6	0.8750	30	77	1.8	330
2016	1	6	0.9167	29.2	77	5.4	290
2016	1	6	0.9583	28.2	82	5.4	310
2016	1	6	1.0000	27.6	87	7.6	310
2016	1	7	0.0417	26.9	89	5.4	290
2016	1	7	0.0833	26.4	91	1.8	300
2016	1	7	0.1250	26.1	94	5.4	280
2016	1	7	0.1667	25.9	95	5.4	310
2016	1	7	0.2083	25.6	96	0	0
2016	1	7	0.2500	25.3	96	0	0
2016	1	7	0.2917	25.1	98	0	0
2016	1	7	0.3333	25.6	96	0	0
2016	1	7	0.3750	27.9	91	1.8	350
2016	1	7	0.4167	29.6	79	9.4	290
2016	1	7	0.4583	31.4	68	9.4	330
2016	1	7	0.5000	31.6	65	9.4	300
2016	1	7	0.5417	33.1	59	9.4	320
2016	1	7	0.5833	34.1	54	13	280
2016	1	7	0.6250	35.5	54	9.4	260
2016	1	7	0.6667	35.4	49	13	240
2016	1	7	0.7083	35.4	49	11.2	280
2016	1	7	0.7500	34.9	51	11.2	290
2016	1	7	0.7917	32.5	60	11.2	320
2016	1	7	0.8333	30.5	70	7.6	290
2016	1	7	0.8750	29.5	75	3.6	330
2016	1	7	0.9167	25.7	70	7.6	360
2016	1	7	0.9583	23.9	86	9.4	140
2016	1	7	1.0000	24.3	83	5.4	300
2016	1	8	0.0417	24.2	84	1.8	10
2016	1	8	0.0833	23.9	90	0	0
2016	1	8	0.1250	24.1	91	1.8	180
2016	1	8	0.1667	24.3	92	0	0
2016	1	8	0.2083	24.3	92	5.4	260
2016	1	8	0.2500				
2016	1	8	0.2917				
2016	1	8	0.3333				
2016	1	8	0.3750	25.1	91		
2016	1	8	0.4167	25.8	89	3.6	50
2016	1	8	0.4583	27.8	78	3.6	20
2016	1	8	0.5000	29.2	76	5.4	10

YYYY	MM	DD	HH24	Air Temperature in degrees C	Relative humidity in percentage %	Wind speed in km/h	Wind direction in degrees true
2017	1	1	0.0417	23.1	96	1.8	350
2017	1	1	0.0833	22.9	98	3.6	30
2017	1	1	0.1250	23.2	98	0	0
2017	1	1	0.1667	22.8	98	3.6	320
2017	1	1	0.2083	22.7	98	9.4	320
2017	1	1	0.2500	22.7	98	7.6	280
2017	1	1	0.2917	22.6	98	9.4	300
2017	1	1	0.3333	22.8	95	13	300
2017	1	1	0.3750	23.3	95	7.6	300
2017	1	1	0.4167	23.6	93	9.4	290
2017	1	1	0.4583	25.2	88	9.4	280
2017	1	1	0.5000	26.5	84	13	290
2017	1	1	0.5417	26.8	89	13	270
2017	1	1	0.5833	27.1	94	13	230
2017	1	1	0.6250	27.1	93	11.2	290
2017	1	1	0.6667	25.6	94	20.5	260
2017	1	1	0.7083	25.7	96	0	0
2017	1	1	0.7500	25.8	93	5.4	300
2017	1	1	0.7917	26.7	94	7.6	310
2017	1	1	0.8333	26.4	96	5.4	320
2017	1	1	0.8750	25.3	96	11.2	300
2017	1	1	0.9167	24.9	98	3.6	280
2017	1	1	0.9583	24.8	98	0	0
2017	1	1	1.0000	24.8	96	5.4	320
2017	1	2	0.0417	24.6	96	5.4	300
2017	1	2	0.0833	24.6	96	5.4	300
2017	1	2	0.1250	24.6	96	5.4	270
2017	1	2	0.1667	24.3	98	9.4	310
2017	1	2	0.2083	24.2	98	7.6	310
2017	1	2	0.2500	24.4	98	5.4	310
2017	1	2	0.2917	24.5	98	5.4	330
2017	1	2	0.3333	24.7	98	5.4	310
2017	1	2	0.3750	25	96	7.6	290
2017	1	2	0.4167	26.4	89	14.8	250
2017	1	2	0.4583	25.8	94	11.2	260
2017	1	2	0.5000	25.9	96	11.2	270
2017	1	2	0.5417	26.7	93	13	260
2017	1	2	0.5833	27.5	94	11.2	270
2017	1	2	0.6250	26.2	94	14.8	270
2017	1	2	0.6667	27.6	85	16.6	240
2017	1	2	0.7083	28.3	79	20.5	230
2017	1	2	0.7500	28	79	11.2	270
2017	1	2	0.7917	27.8	79	9.4	290
2017	1	2	0.8333	27.4	81	11.2	280
2017	1	2	0.8750	25.8	92	7.6	300
2017	1	2	0.9167	25.4	92	11.2	300
2017	1	2	0.9583	25.3	91	9.4	310
2017	1	2	1.0000	25.1	93	7.6	300
2017	1	3	0.0417	24.8	96	5.4	330
2017	1	3	0.0833	24.9	96	3.6	350
2017	1	3	0.1250	24.8	96	1.8	350
2017	1	3	0.1667	24.8	98	3.6	30
2017	1	3	0.2083	24.8	98	0	0
2017	1	3	0.2500	24.8	98	1.8	30
2017	1	3	0.2917	24.8	98	1.8	40
2017	1	3	0.3333	24.9	98	5.4	40
2017	1	3	0.3750	25.8	95	7.6	40
2017	1	3	0.4167	26.8	90	7.6	50
2017	1	3	0.4583	27.4	86	5.4	30
2017	1	3	0.5000	27.4	90	1.8	10
2017	1	3	0.5417	27.8	84	9.4	50
2017	1	3	0.5833	28.7	84	7.6	50
2017	1	3	0.6250	29	82	5.4	30
2017	1	3	0.6667	26.1	96	9.4	20
2017	1	3	0.7083	27.2	93	5.4	30
2017	1	3	0.7500	27.6	90	5.4	20
2017	1	3	0.7917	27.6	90	5.4	30
2017	1	3	0.8333	26.5	92	5.4	10
2017	1	3	0.8750	26.3	94	3.6	10
2017	1	3	0.9167	26	94	3.6	10
2017	1	3	0.9583	25.8	94	5.4	10
2017	1	3	1.0000	25.9	93	1.8	10
2017	1	4	0.0417	25.6	94	1.8	360
2017	1	4	0.0833	25.4	94	0	0
2017	1	4	0.1250	25.1	96	0	0
2017	1	4	0.1667	25.2	96	0	0
2017	1	4	0.2083	25.7	94	0	0
2017	1	4	0.2500	25.5	96	7.6	50
2017	1	4	0.2917	25.5	96	5.4	50
2017	1	4	0.3333	25.9	95	5.4	30
2017	1	4	0.3750	27.7	87	7.6	30
2017	1	4	0.4167	27	91	5.4	10
2017	1	4	0.4583	29.2	83	9.4	20
2017	1	4	0.5000	30.8	72	9.4	360
2017	1	4	0.5417	32.3	66	13	350
2017	1	4	0.5833	32.7	66	13	340
2017	1	4	0.6250	29	85	9.4	10
2017	1	4	0.6667	31.8	67	11.2	330
2017	1	4	0.7083	31.8	62	9.4	360
2017	1	4	0.7500	31.7	67	5.4	350
2017	1	4	0.7917	27.3	93	3.6	360
2017	1	4	0.8333	27.4	91	3.6	10
2017	1	4	0.8750	26.8	94	0	0
2017	1	4	0.9167	26.7	92	1.8	340
2017	1	4	0.9583	26.2	96	0	0
2017	1	4	1.0000	25.9	95	0	0
2017	1	5	0.0417	25.5	96	0	0
2017	1	5	0.0833	25.3	96	0	0
2017	1	5	0.1250	25.2	96	0	0
2017	1	5	0.1667	25.1	96	0	0
2017	1	5	0.2083	24.8	98	0	0
2017	1	5	0.2500	24.6	98	0	0
2017	1	5	0.2917	24.6	98	0	0
2017	1	5	0.3333	25.1	98	0	0
2017	1	5	0.3750	27.7	90	1.8	60
2017	1	5	0.4167	29.2	80	9.4	320
2017	1	5	0.4583	30.3	74	7.6	310
2017	1	5	0.5000	30.2	78	5.4	330
2017	1	5	0.5417	31	69	11.2	320
2017	1	5	0.5833	30.9	67	11.2	320
2017	1	5	0.6250	27.8	87	22.3	240
2017	1	5	0.6667	27.4	91	1.8	30
2017	1	5	0.7083	26.1	91	24.1	260
2017	1	5	0.7500	26.4	89	0	0
2017	1	5	0.7917	26.9	89	1.8	60
2017	1	5	0.8333	26.2	96	1.8	360
2017	1	5	0.8750	25.4	96	5.4	10
2017	1	5	0.9167	25.4	96	0	0
2017	1	5	0.9583	25.3	98	0	0
2017	1	5	1.0000	25.3	98	0	0
2017	1	6	0.0417	25.2	98	0	0
2017	1	6	0.0833	24.9	98	0	0
2017	1	6	0.1250	24.9	98	0	0
2017	1	6	0.1667	24.8	98	0	0
2017	1	6	0.2083	24.6	98	0	0
2017	1	6	0.2500	24.5	98	0	0
2017	1	6	0.2917	24.5	98	0	0
2017	1	6	0.3333	24.9	98	0	0
2017	1	6	0.3750	26.2	96	0	0
2017	1	6	0.4167	28.4	88	7.6	320
2017	1	6	0.4583	29.3	79	9.4	280
2017	1	6	0.5000	30.6	79	9.4	270
2017	1	6	0.5417	31.7	67	18.4	240
2017	1	6	0.5833	32.3	65	16.6	250
2017	1	6	0.6250	31.5	60	20.5	260
2017	1	6	0.6667	32.7	59	16.6	260
2017	1	6	0.7083	32.6	59	18.4	270
2017	1	6	0.7500	31.7	60	14.8	270
2017	1	6	0.7917	32.2	59	11.2	270
2017	1	6	0.8333	30.5	66	9.4	290
2017	1	6	0.8750	29	76	9.4	290
2017	1	6	0.9167	28	81	7.6	300
2017	1	6	0.9583	27.2	86	7.6	310
2017	1	6	1.0000	26.4	91	3.6	320
2017	1	7	0.0417	25.7	94	3.6	310
2017	1	7	0.0833	25.7	95	7.6	320
2017	1	7	0.1250	25.4	96	5.4	310
2017	1	7	0.1667	25.3	96	0	0
2017	1	7	0.2083	24.9	98	0	0
2017	1	7	0.2500	24.7	98	0	0
2017	1	7	0.2917	24.9	98	1.8	350
2017	1	7	0.3333	25.3	98	0	0
2017	1	7	0.3750	26.7	94	5.4	290
2017	1	7	0.4167	28.9	84	13	290
2017	1	7	0.4583	29.6	73	14.8	260
2017	1	7	0.5000	30.9	68	18.4	240
2017	1	7	0.5417	31.4	63	16.6	270
2017	1	7	0.5833	32	58	16.6	260
2017	1	7	0.6250	32.5	62	13	250
2017	1	7	0.6667	33.4	55	14.8	270
2017	1	7	0.7083	33.7	54	16.6	270
2017	1	7	0.7500	32.6	57	13	280
2017	1	7	0.7917	31.8	63	11.2	300
2017	1	7	0.8333	30.5	67	11.2	280
2017	1	7	0.8750	29.4	71	9.4	300
2017	1	7	0.9167	28.5	78	7.6	310
2017	1	7	0.9583	27.8	82	5.4	300
2017	1	7	1.0000	27.3	86	7.6	310
2017	1	8	0.0417	26.8	91	3.6	310
2017	1	8	0.0833	26.4	94	1.8	310
2017	1	8	0.1250	26.2	94	0	0
2017	1	8	0.1667	26	96	0	0
2017	1	8	0.2083	26.1	96	3.6	330
2017	1	8	0.2500	26.1	96	1.8	350
2017	1	8	0.2917	25.9	97	1.8	290
2017	1	8	0.3333	26.2	96	0	0
2017	1	8	0.3750	28.1	87	7.6	280
2017	1	8	0.4167	29.6	77	20.5	250
2017	1	8	0.4583	30.9	68	20.5	250
2017	1	8	0.5000	31.4	66	16.6	250

YYYY	MM	DD	HH24	Air Temperature in degrees C	Relative humidity in percentage %	Wind speed in km/h	Wind direction in degrees true
2018	1	1	0.0417	27.6	87	3.6	330
2018	1	1	0.0833	27	91	0	0
2018	1	1	0.1250	26.6	92	3.6	20
2018	1	1	0.1667	26.4	94	0	0
2018	1	1	0.2083	26.2	94	0	0
2018	1	1	0.2500	26.4	93	7.6	350
2018	1	1	0.2917	26.1	93	0	0
2018	1	1	0.3333	26.8	92	1.8	310
2018	1	1	0.3750	28.1	86	3.6	280
2018	1	1	0.4167	30.7	76	5.4	320
2018	1	1	0.4583	32.1	66	11.2	280
2018	1	1	0.5000	33.1	61	9.4	270
2018	1	1	0.5417	33.1	61	9.4	280
2018	1	1	0.5833	34.2	55	9.4	290
2018	1	1	0.6250	35.3	54	7.6	240
2018	1	1	0.6667	36.1	48	7.6	310
2018	1	1	0.7083	33.8	58	18.4	330
2018	1	1	0.7500	34.1	60	14.8	340
2018	1	1	0.7917	29.5	71	18.4	310
2018	1	1	0.8333	28	74	11.2	340
2018	1	1	0.8750	27.5	84	3.6	40
2018	1	1	0.9167	26.8	88	5.4	210
2018	1	1	0.9583	26.7	89	5.4	340
2018	1	1	1.0000	26.4	91	1.8	360
2018	1	2	0.0417	26.1	92	7.6	30
2018	1	2	0.0833	26	92	3.6	230
2018	1	2	0.1250	25.7	93	0	0
2018	1	2	0.1667	25.7	94	0	0
2018	1	2	0.2083	25.9	94	0	0
2018	1	2	0.2500	25.8	94	0	0
2018	1	2	0.2917	25.7	95	0	0
2018	1	2	0.3333	26	94	0	0
2018	1	2	0.3750	27.6	90	5.4	360
2018	1	2	0.4167	30	79	1.8	280
2018	1	2	0.4583	31.7	72	5.4	250
2018	1	2	0.5000	32.9	61	9.4	250
2018	1	2	0.5417	33.5	58	7.6	300
2018	1	2	0.5833	34.3	54	9.4	260
2018	1	2	0.6250	35.3	50	11.2	290
2018	1	2	0.6667	35.6	52	13	260
2018	1	2	0.7083	35.8	51	11.2	290
2018	1	2	0.7500	30	67	11.2	350
2018	1	2	0.7917	30	70	14.8	350
2018	1	2	0.8333	29	74	11.2	340
2018	1	2	0.8750	28.2	78	9.4	340
2018	1	2	0.9167	27.5	82	5.4	350
2018	1	2	0.9583	27	86	3.6	290
2018	1	2	1.0000	26.9	86	11.2	350
2018	1	3	0.0417	27	87	5.4	330
2018	1	3	0.0833	26.6	90	0	0
2018	1	3	0.1250	26.6	91	5.4	340
2018	1	3	0.1667	25.8	88	22.3	90
2018	1	3	0.2083	23.9	90	20.5	100
2018	1	3	0.2500	23.3	92	22.3	120
2018	1	3	0.2917	23.2	94	11.2	210
2018	1	3	0.3333	23.2	93	9.4	230
2018	1	3	0.3750	23.1	93	5.4	250
2018	1	3	0.4167	23.4	91	3.6	20
2018	1	3	0.4583	24.4	89	7.6	70
2018	1	3	0.5000	25.8	85	9.4	80
2018	1	3	0.5417	27.5	77	9.4	70
2018	1	3	0.5833	29.9	72	9.4	70
2018	1	3	0.6250	30.6	66	14.8	130
2018	1	3	0.6667	28.9	70	18.4	140
2018	1	3	0.7083	29	69	14.8	140
2018	1	3	0.7500	29.9	69	11.2	130
2018	1	3	0.7917	30.2	67	9.4	130
2018	1	3	0.8333	30.3	71	5.4	230
2018	1	3	0.8750	28.5	79	5.4	270
2018	1	3	0.9167	27.9	83	0	0
2018	1	3	0.9583	27.3	86	0	0
2018	1	3	1.0000	27.2	84	7.6	340
2018	1	4	0.0417	26.7	87	5.4	330
2018	1	4	0.0833	26.3	89	5.4	330
2018	1	4	0.1250	26.3	89	7.6	350
2018	1	4	0.1667	25.4	92	3.6	270
2018	1	4	0.2083	25.2	94	1.8	130
2018	1	4	0.2500	25	94	5.4	30
2018	1	4	0.2917	24.9	93	5.4	330
2018	1	4	0.3333	25.6	92	1.8	300
2018	1	4	0.3750	26.5	90	0	0
2018	1	4	0.4167	28	84	0	0
2018	1	4	0.4583	29.5	82	5.4	200
2018	1	4	0.5000	31.8	66	5.4	270
2018	1	4	0.5417	33.1	55	11.2	260
2018	1	4	0.5833	33.8	56	11.2	260
2018	1	4	0.6250	34.8	57	11.2	270
2018	1	4	0.6667	35.2	53	13	250
2018	1	4	0.7083	33.3	58	11.2	330
2018	1	4	0.7500	23.9	95	31.3	110
2018	1	4	0.7917	24.1	94	14.8	100
2018	1	4	0.8333	24	95	5.4	350
2018	1	4	0.8750	23.8	95	7.6	290
2018	1	4	0.9167	23.7	95	7.6	270
2018	1	4	0.9583	23.8	96	5.4	220
2018	1	4	1.0000	23.8	96	9.4	100
2018	1	5	0.0417	23.6	95	5.4	60
2018	1	5	0.0833	23.5	95	0	0
2018	1	5	0.1250	23.5	95	0	0
2018	1	5	0.1667	23.4	96	5.4	300
2018	1	5	0.2083	23.5	96	0	0
2018	1	5	0.2500	23.5	96	0	0
2018	1	5	0.2917	23.4	97	9.4	130
2018	1	5	0.3333	24	96	9.4	110
2018	1	5	0.3750	25.7	88	7.6	140
2018	1	5	0.4167	26.6	83	5.4	100
2018	1	5	0.4583	28.8	77	5.4	160
2018	1	5	0.5000	30.1	70	7.6	190
2018	1	5	0.5417	30.9	66	5.4	110
2018	1	5	0.5833	32	58	9.4	350
2018	1	5	0.6250	33.6	59	9.4	330
2018	1	5	0.6667	34	47	9.4	250
2018	1	5	0.7083	33.7	50	5.4	270
2018	1	5	0.7500	29	63	22.3	160
2018	1	5	0.7917	29.5	68	7.6	20
2018	1	5	0.8333	26.3	77	11.2	10
2018	1	5	0.8750	24.9	79	13	360
2018	1	5	0.9167	23.2	96	11.2	60
2018	1	5	0.9583	23.7	96	7.6	60
2018	1	5	1.0000	23.7	96	0	0
2018	1	6	0.0417	23.4	95	7.6	350
2018	1	6	0.0833	23.4	95	7.6	340
2018	1	6	0.1250	23.5	94	0	0
2018	1	6	0.1667	23.4	94	0	0
2018	1	6	0.2083	23.3	95	9.4	190
2018	1	6	0.2500	23.3	96	7.6	200
2018	1	6	0.2917	23	95	5.4	140
2018	1	6	0.3333	23.4	96	7.6	80
2018	1	6	0.3750	24.3	92	11.2	120
2018	1	6	0.4167	24.9	89	11.2	130
2018	1	6	0.4583	26.1	86	11.2	130
2018	1	6	0.5000	26.7	79	9.4	110
2018	1	6	0.5417	28.7	75	11.2	110
2018	1	6	0.5833	29.9	67	5.4	100
2018	1	6	0.6250	30.4	64	11.2	140
2018	1	6	0.6667	30.1	69	13	80
2018	1	6	0.7083	30.1	66	13	90
2018	1	6	0.7500	31.1	67	13	130
2018	1	6	0.7917	30.5	65	13	110
2018	1	6	0.8333	24.5	90	11.2	360
2018	1	6	0.8750	24.4	91	0	0
2018	1	6	0.9167	24.5	93	1.8	100
2018	1	6	0.9583	24.7	93	0	0
2018	1	6	1.0000	24.7	94	9.4	120
2018	1	7	0.0417	24.9	93	9.4	130
2018	1	7	0.0833	24.7	93	11.2	130
2018	1	7	0.1250	24.3	93	14.8	140
2018	1	7	0.1667	24	95	9.4	120
2018	1	7	0.2083	24	95	9.4	110
2018	1	7	0.2500	24.1	94	5.4	60
2018	1	7	0.2917	24.1	95	0	0
2018	1	7	0.3333	24.4	96	0	0
2018	1	7	0.3750	25.4	95	7.6	110
2018	1	7	0.4167	26.8	86	9.4	50
2018	1	7	0.4583	28.2	78	9.4	30
2018	1	7	0.5000	29.3	76	9.4	40
2018	1	7	0.5417	29.4	71	13	20
2018	1	7	0.5833	30.1	67	16.6	10
2018	1	7	0.6250	30.1	68	16.6	360
2018	1	7	0.6667	29.4	74	16.6	360
2018	1	7	0.7083	29.2	71	14.8	360
2018	1	7	0.7500	28.2	73	13	20
2018	1	7	0.7917	27.8	76	11.2	10
2018	1	7	0.8333	27.2	79	9.4	30
2018	1	7	0.8750	26.4	83	9.4	30
2018	1	7	0.9167	25.8	85	5.4	30
2018	1	7	0.9583	25.6	86	9.4	30
2018	1	7	1.0000	25.3	88	5.4	50
2018	1	8	0.0417	25.1	90	0	0
2018	1	8	0.0833	25.2	91	5.4	30
2018	1	8	0.1250	25.1	91	5.4	60
2018	1	8	0.1667	25.1	91	3.6	30
2018	1	8	0.2083	24.9	91	7.6	40
2018	1	8	0.2500	25	90	7.6	30
2018	1	8	0.2917	24.8	90	3.6	360
2018	1	8	0.3333	24.9	90	3.6	20
2018	1	8	0.3750	25.6	86	7.6	10
2018	1	8	0.4167	27.8	78	7.6	20
2018	1	8	0.4583	29.2	72	7.6	350
2018	1	8	0.5000	31	64	13	350

YYYY	MM	DD	HH24	Air Temperature in degrees C	Relative humidity in percentage %	Wind speed in km/h	Wind direction in degrees true
2019	1	1	0.0417	24.8	93	0	0
2019	1	1	0.0833	24.7	94	9.4	340
2019	1	1	0.1250	24.7	94	13	340
2019	1	1	0.1667	24.7	91	13	330
2019	1	1	0.2083	25	90	5.4	30
2019	1	1	0.2500	25	92	0	0
2019	1	1	0.2917	24.7	93	5.4	210
2019	1	1	0.3333	24.9	93	0	0
2019	1	1	0.3750	26.3	89	3.6	130
2019	1	1	0.4167	28.1	78	5.4	340
2019	1	1	0.4583	29.4	78	9.4	310
2019	1	1	0.5000	31	72	18.4	260
2019	1	1	0.5417	32.2	65	18.4	310
2019	1	1	0.5833	33.5	60	16.6	270
2019	1	1	0.6250	34.8	57	13	270
2019	1	1	0.6667	34.2	53	18.4	270
2019	1	1	0.7083	34.3	54	16.6	320
2019	1	1	0.7500	31.6	64	20.5	300
2019	1	1	0.7917	31.2	70	13	340
2019	1	1	0.8333	30.6	70	11.2	340
2019	1	1	0.8750	29.6	75	13	350
2019	1	1	0.9167	28.8	79	9.4	340
2019	1	1	0.9583	28.1	83	7.6	340
2019	1	1	1.0000	27.2	85	7.6	350
2019	1	2	0.0417	26.7	90	9.4	130
2019	1	2	0.0833	27	87	1.8	80
2019	1	2	0.1250	26.8	87	0	0
2019	1	2	0.1667	26.7	90	13	340
2019	1	2	0.2083	27.2	89	13	290
2019	1	2	0.2500	27.8	87	9.4	300
2019	1	2	0.2917	27.8	87	7.6	320
2019	1	2	0.3333	27.8	87	7.6	320
2019	1	2	0.3750	29.4	81	11.2	310
2019	1	2	0.4167	30.7	73	14.8	290
2019	1	2	0.4583	31.3	71	16.6	270
2019	1	2	0.5000	32	67	14.8	290
2019	1	2	0.5417	33.6	59	16.6	270
2019	1	2	0.5833	33.8	64	11.2	320
2019	1	2	0.6250	34.2	57	11.2	310
2019	1	2	0.6667	35.7	54	13	310
2019	1	2	0.7083	35.4	50	13	320
2019	1	2	0.7500	35.2	51	13	320
2019	1	2	0.7917	33.1	54	16.6	320
2019	1	2	0.8333	31.5	62	13	310
2019	1	2	0.8750	30	69	7.6	330
2019	1	2	0.9167	29.2	71	13	310
2019	1	2	0.9583	28.3	77	9.4	320
2019	1	2	1.0000	27.6	83	9.4	330
2019	1	3	0.0417	27.4	86	5.4	330
2019	1	3	0.0833	26.9	89	7.6	340
2019	1	3	0.1250	26.7	90	7.6	350
2019	1	3	0.1667	26.4	90	7.6	320
2019	1	3	0.2083	26.2	91	5.4	310
2019	1	3	0.2500	25.9	93	3.6	350
2019	1	3	0.2917	26	93	7.6	340
2019	1	3	0.3333	26.3	92	5.4	360
2019	1	3	0.3750	28.5	84	7.6	330
2019	1	3	0.4167	29.8	80	11.2	310
2019	1	3	0.4583	31.6	64	16.6	310
2019	1	3	0.5000	32.4	59	14.8	300
2019	1	3	0.5417	34.4	56	20.5	280
2019	1	3	0.5833	34.5	53	18.4	290
2019	1	3	0.6250	35.5	49	16.6	280
2019	1	3	0.6667	35.4	49	16.6	290
2019	1	3	0.7083	36.1	47	13	290
2019	1	3	0.7500	34.4	51	16.6	310
2019	1	3	0.7917	34	55	14.8	320
2019	1	3	0.8333	32.1	61	14.8	310
2019	1	3	0.8750	30.5	66	11.2	310
2019	1	3	0.9167	29.5	71	13	310
2019	1	3	0.9583	28.7	78	9.4	310
2019	1	3	1.0000	28.2	83	7.6	320
2019	1	4	0.0417	28.3	83	7.6	310
2019	1	4	0.0833	27.9	86	11.2	330
2019	1	4	0.1250	27.7	88	16.6	340
2019	1	4	0.1667	28.1	86	11.2	310
2019	1	4	0.2083	28.2	83	11.2	330
2019	1	4	0.2500	28	85	5.4	200
2019	1	4	0.2917	27.5	88	11.2	270
2019	1	4	0.3333	25.5	88	14.8	200
2019	1	4	0.3750	25.9	86	7.6	130
2019	1	4	0.4167	26.1	83	20.5	100
2019	1	4	0.4583	26.6	76	18.4	90
2019	1	4	0.5000	27	73	9.4	340
2019	1	4	0.5417	28	75	5.4	360
2019	1	4	0.5833	30.3	66	5.4	50
2019	1	4	0.6250	31.9	60	9.4	280
2019	1	4	0.6667	33.3	62	13	280
2019	1	4	0.7083	34.2	53	14.8	260
2019	1	4	0.7500	33.9	54	9.4	270
2019	1	4	0.7917	33.2	57	9.4	190
2019	1	4	0.8333	31.1	66	14.8	250
2019	1	4	0.8750	29.4	70	16.6	270
2019	1	4	0.9167	28.4	72	9.4	310
2019	1	4	0.9583	27.2	80	9.4	320
2019	1	4	1.0000	26.7	81	7.6	310
2019	1	5	0.0417	25.8	85	5.4	320
2019	1	5	0.0833	25.3	89	3.6	310
2019	1	5	0.1250	25	89	0	0
2019	1	5	0.1667	25	90	3.6	290
2019	1	5	0.2083	24.7	91	1.8	340
2019	1	5	0.2500	24.5	91	0	0
2019	1	5	0.2917	24.1	94	0	0
2019	1	5	0.3333	24.5	94	5.4	70
2019	1	5	0.3750	25.8	91	7.6	10
2019	1	5	0.4167	29	78	7.6	200
2019	1	5	0.4583	30.4	71	9.4	260
2019	1	5	0.5000	31.9	64	7.6	10
2019	1	5	0.5417	33.1	63	9.4	320
2019	1	5	0.5833	34.9	49	11.2	230
2019	1	5	0.6250	35.7	47	9.4	270
2019	1	5	0.6667	37.2	41	11.2	220
2019	1	5	0.7083	37.7	43	5.4	290
2019	1	5	0.7500	37.5	39	7.6	300
2019	1	5	0.7917	36.4	47	9.4	320
2019	1	5	0.8333	32.9	63	14.8	330
2019	1	5	0.8750	30.3	71	14.8	320
2019	1	5	0.9167	29.5	75	5.4	310
2019	1	5	0.9583	27.8	82	7.6	330
2019	1	5	1.0000	27.1	87	9.4	340
2019	1	6	0.0417	26.8	89	7.6	330
2019	1	6	0.0833	26.7	88	9.4	330
2019	1	6	0.1250	26.3	89	5.4	350
2019	1	6	0.1667	21.7	94	5.4	70
2019	1	6	0.2083	22.1	96	3.6	160
2019	1	6	0.2500	22	96	7.6	320
2019	1	6	0.2917	22.3	94	7.6	310
2019	1	6	0.3333	22.6	94	5.4	80
2019	1	6	0.3750	22.8	93	7.6	20
2019	1	6	0.4167	24.2	89	0	0
2019	1	6	0.4583	25.7	80	3.6	320
2019	1	6	0.5000	27.7	74	3.6	110
2019	1	6	0.5417	30.1	64	7.6	200
2019	1	6	0.5833	32.8	59	9.4	270
2019	1	6	0.6250	33.1	54	7.6	290
2019	1	6	0.6667	33.9	45	7.6	190
2019	1	6	0.7083	33.8	47	5.4	340
2019	1	6	0.7500	33.2	56	5.4	320
2019	1	6	0.7917	31.5	67	13	270
2019	1	6	0.8333	29.4	73	9.4	290
2019	1	6	0.8750	28.5	77	5.4	310
2019	1	6	0.9167	27.8	80	5.4	310
2019	1	6	0.9583	27	85	7.6	340
2019	1	6	1.0000	26.6	87	5.4	350
2019	1	7	0.0417	25.8	90	0	0
2019	1	7	0.0833	25.2	93	0	0
2019	1	7	0.1250	25.4	92	0	0
2019	1	7	0.1667	25	92	0	0
2019	1	7	0.2083	24.7	95	18.4	120
2019	1	7	0.2500	24.9	94	0	0
2019	1	7	0.2917	24.5	95	3.6	250
2019	1	7	0.3333	24.8	95	5.4	240
2019	1	7	0.3750	26.7	85	7.6	280
2019	1	7	0.4167	28.2	76	0	0
2019	1	7	0.4583	31	60	7.6	230
2019	1	7	0.5000	32.1	54	11.2	230
2019	1	7	0.5417	32.1	53	7.6	230
2019	1	7	0.5833	33	52	5.4	360
2019	1	7	0.6250	34.3	47	9.4	300
2019	1	7	0.6667	35.9	44	9.4	290
2019	1	7	0.7083	37.2	38	1.8	290
2019	1	7	0.7500	37	35	5.4	270
2019	1	7	0.7917	36.9	37	5.4	310
2019	1	7	0.8333	33.9	52	0	0
2019	1	7	0.8750	30.5	63	3.6	330
2019	1	7	0.9167	29.1	74	5.4	340
2019	1	7	0.9583	29.2	77	13	310
2019	1	7	1.0000	28.6	84	9.4	320
2019	1	8	0.0417	28	88	7.6	320
2019	1	8	0.0833	27.2	91	5.4	320
2019	1	8	0.1250	26.4	92	1.8	290
2019	1	8	0.1667	26.5	93	5.4	330
2019	1	8	0.2083	26.4	92	5.4	300
2019	1	8	0.2500	25.8	94	5.4	350
2019	1	8	0.2917	26.1	94	5.4	330
2019	1	8	0.3333	26.4	94	9.4	330
2019	1	8	0.3750	27.9	88	7.6	340
2019	1	8	0.4167	29.8	83	7.6	320
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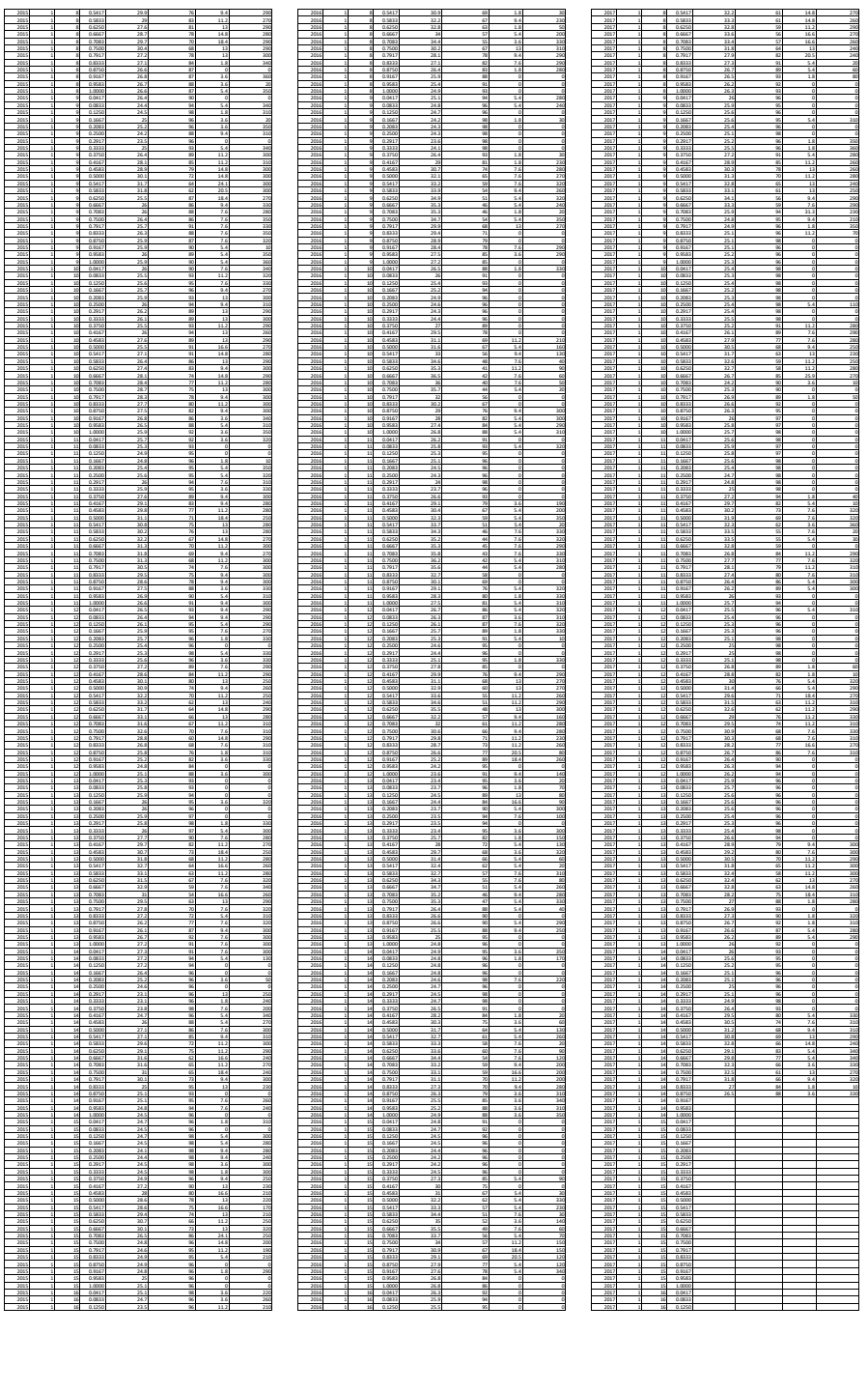

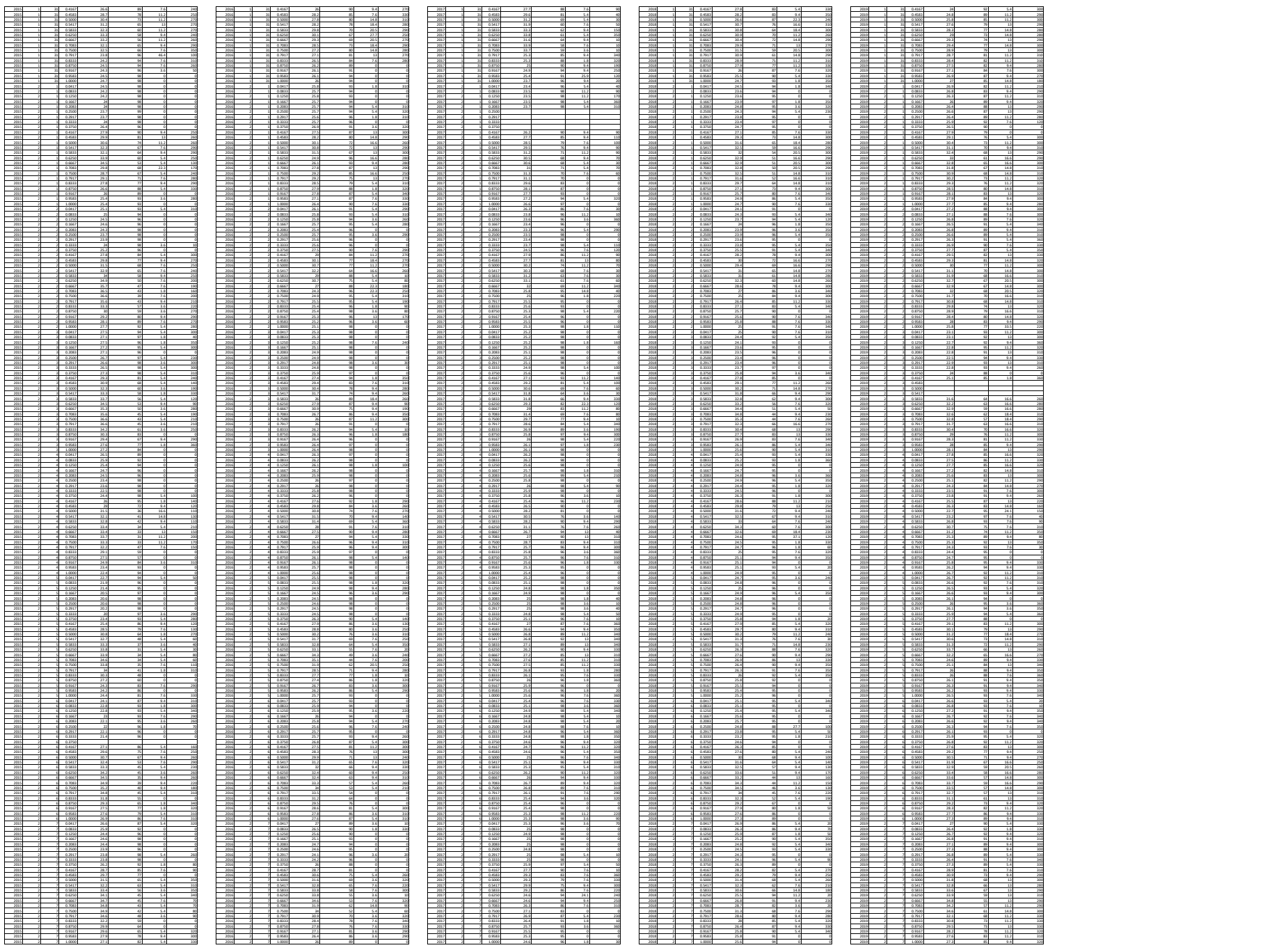

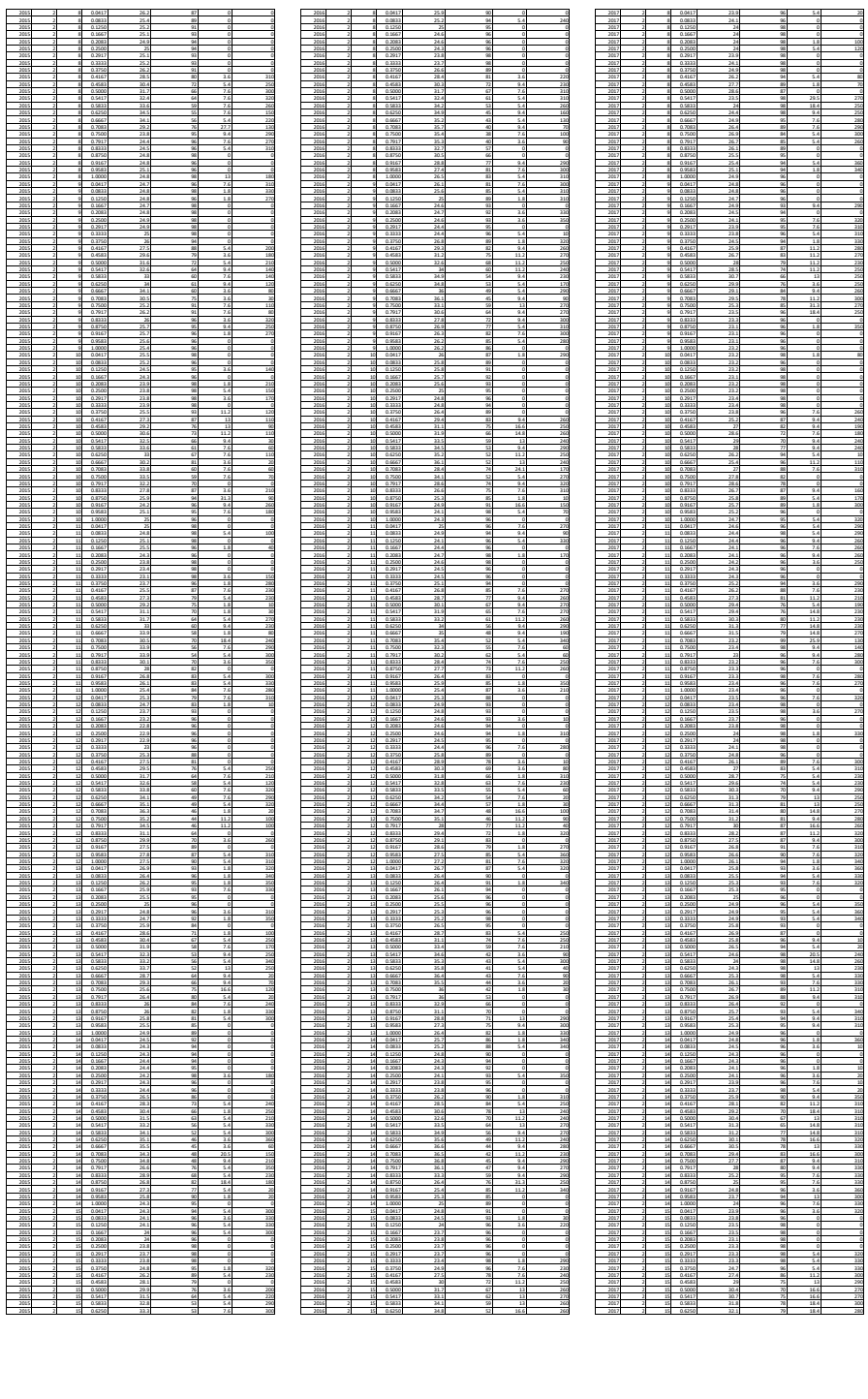

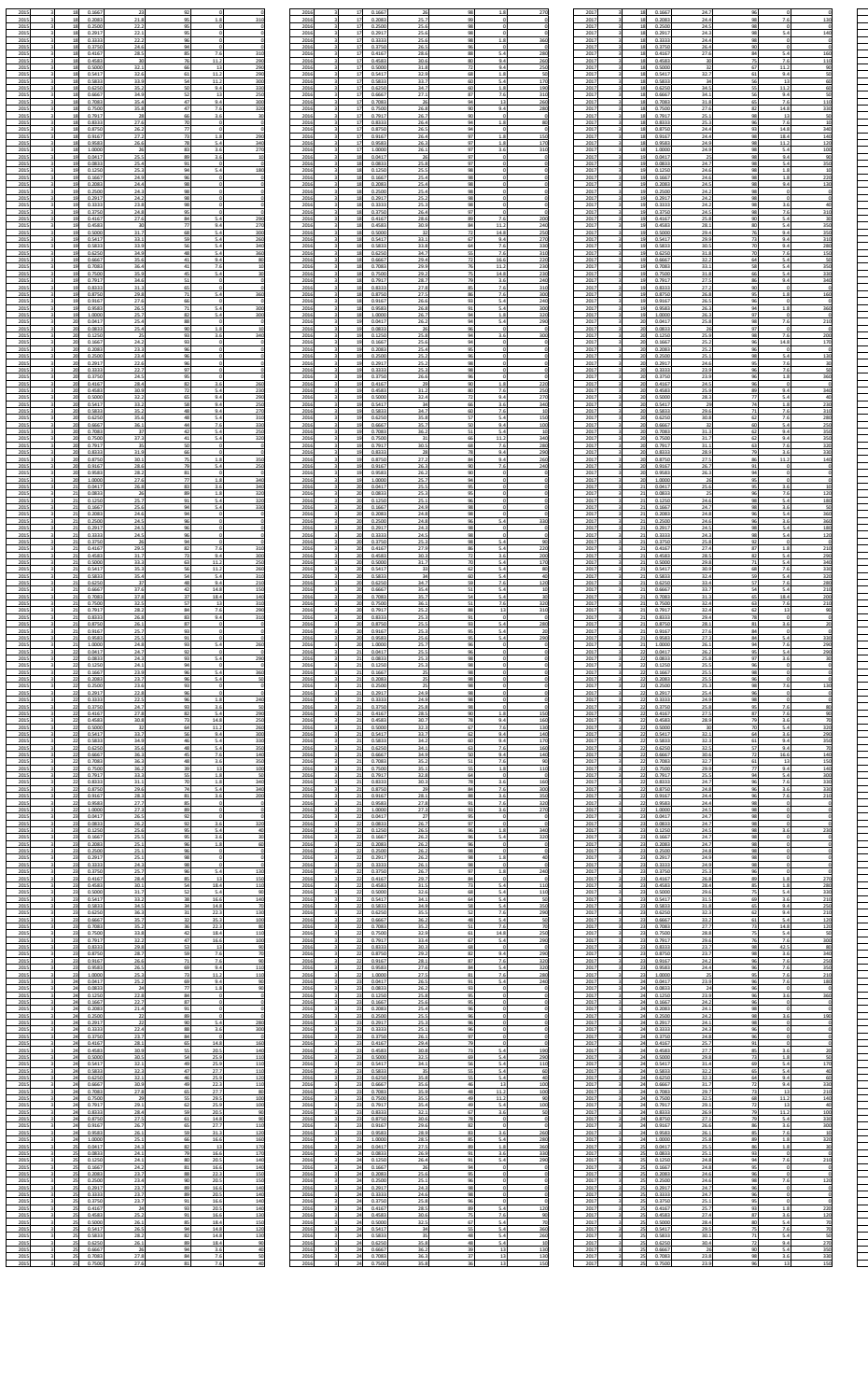

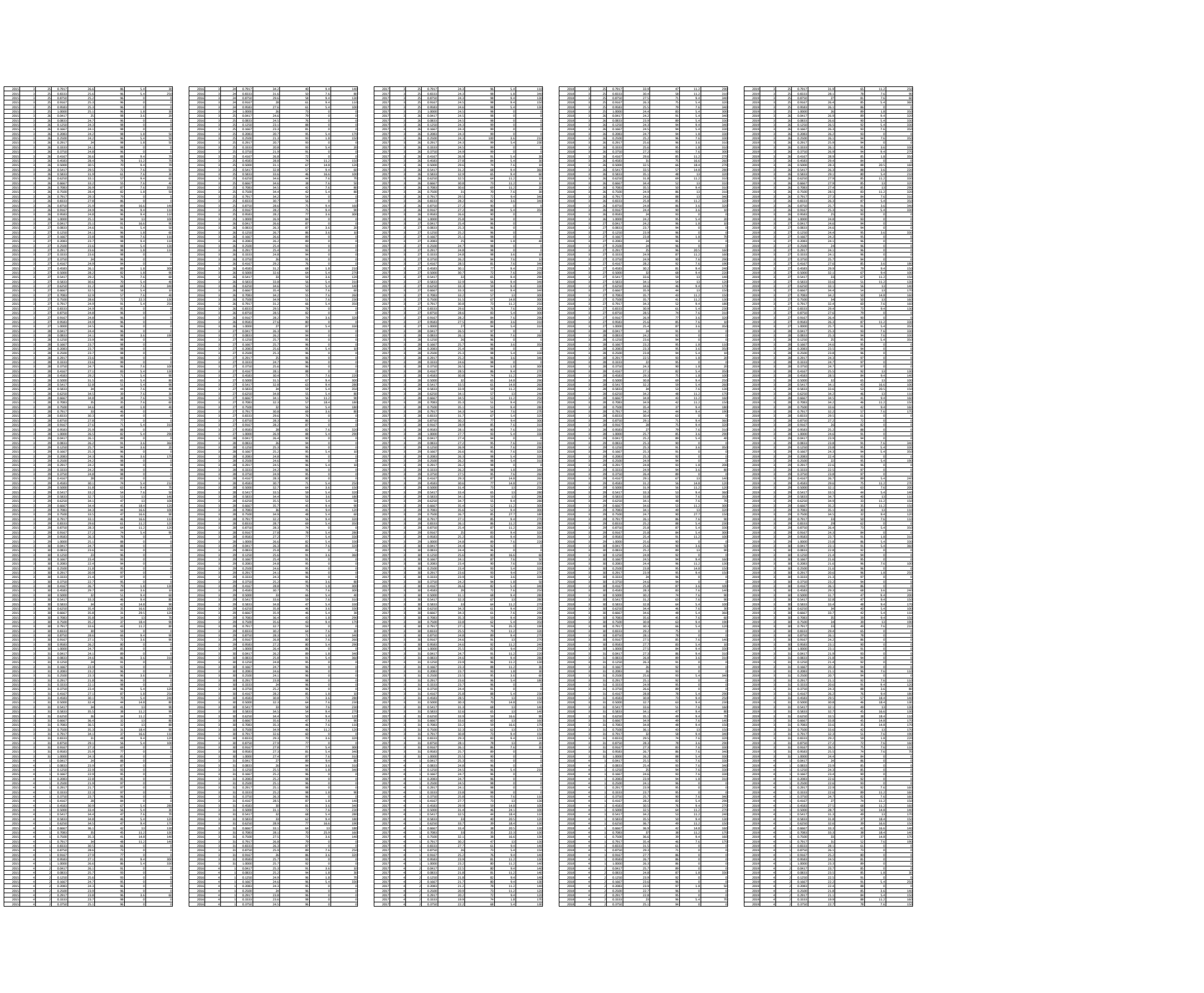

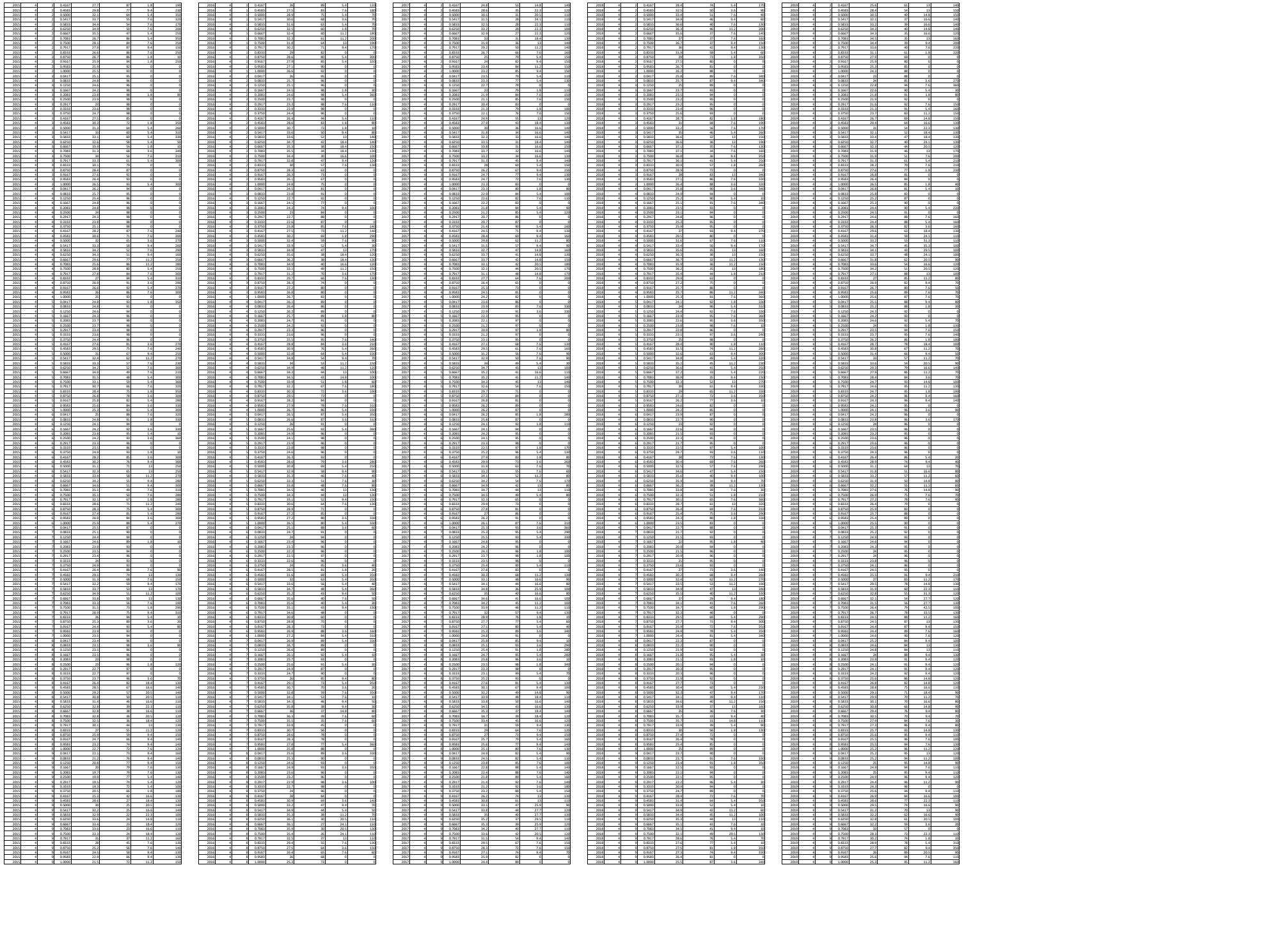

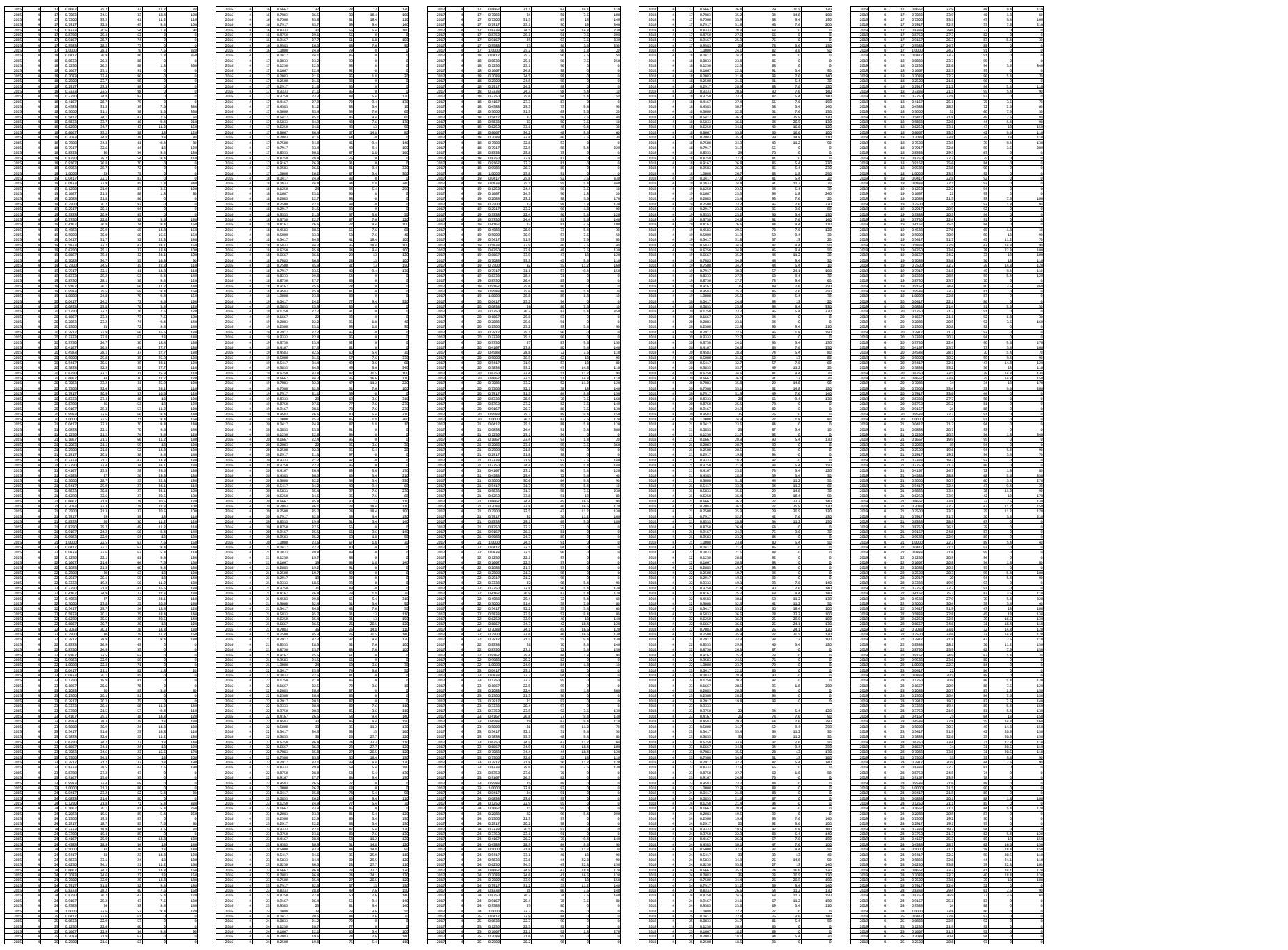

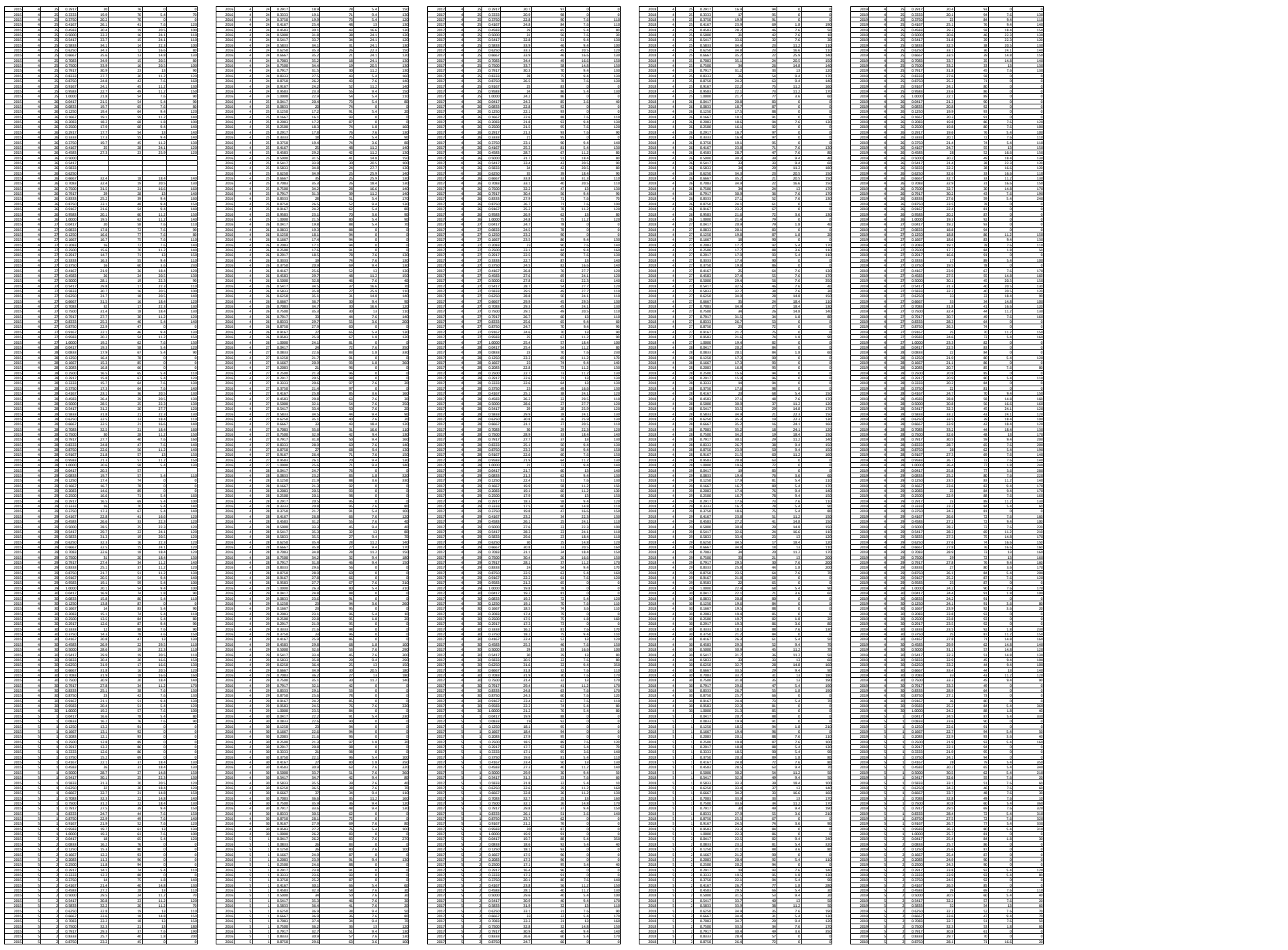

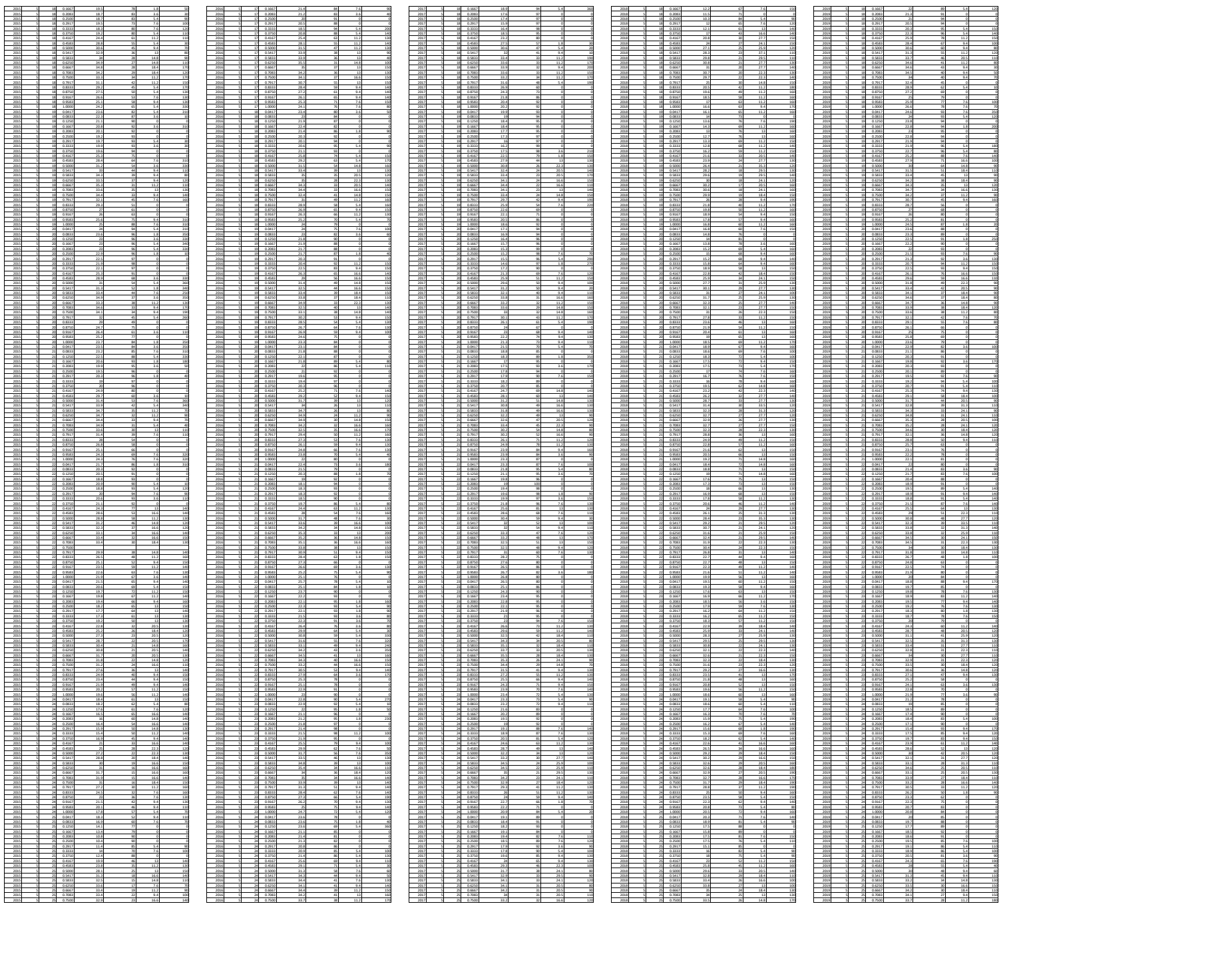

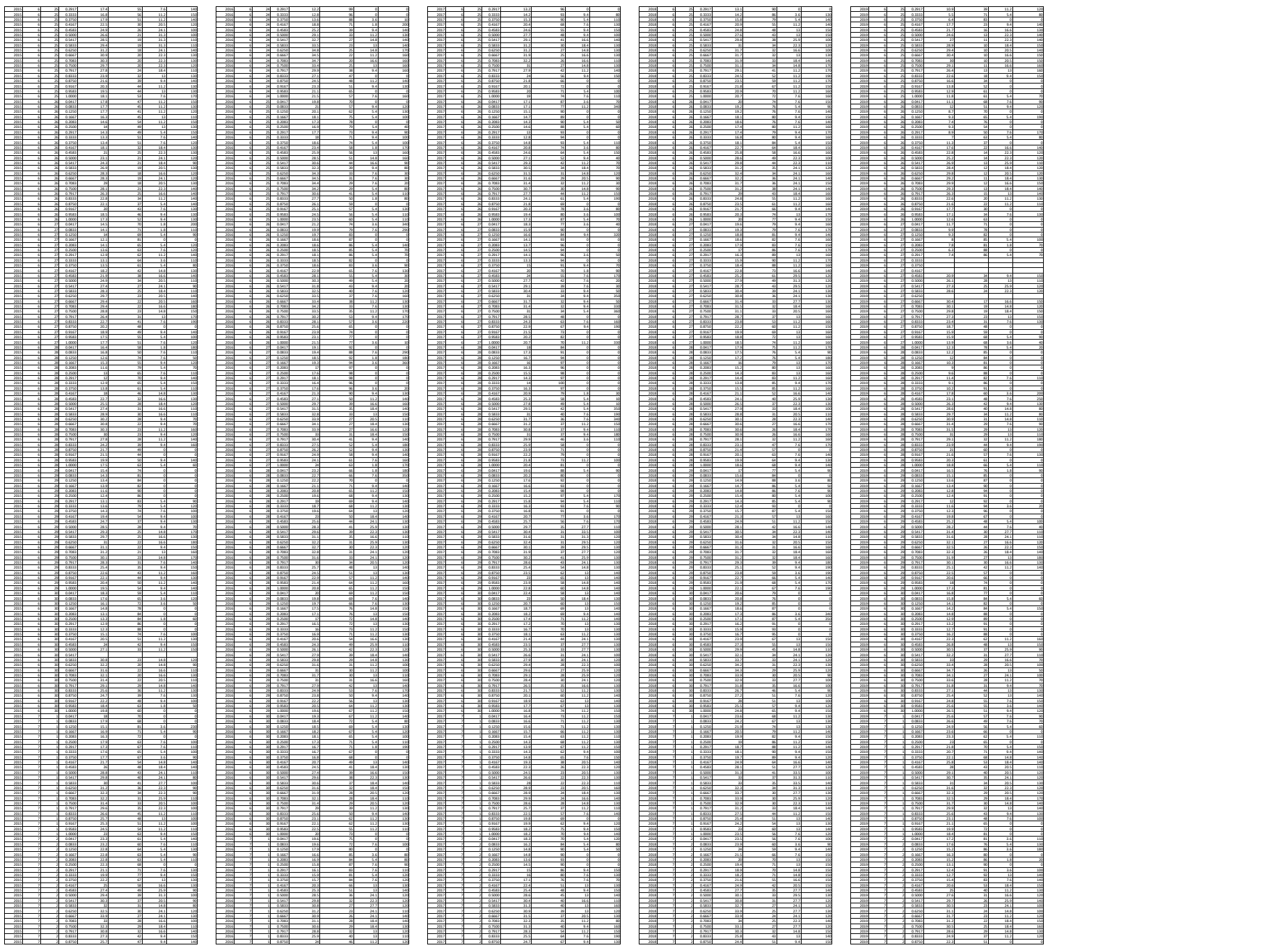

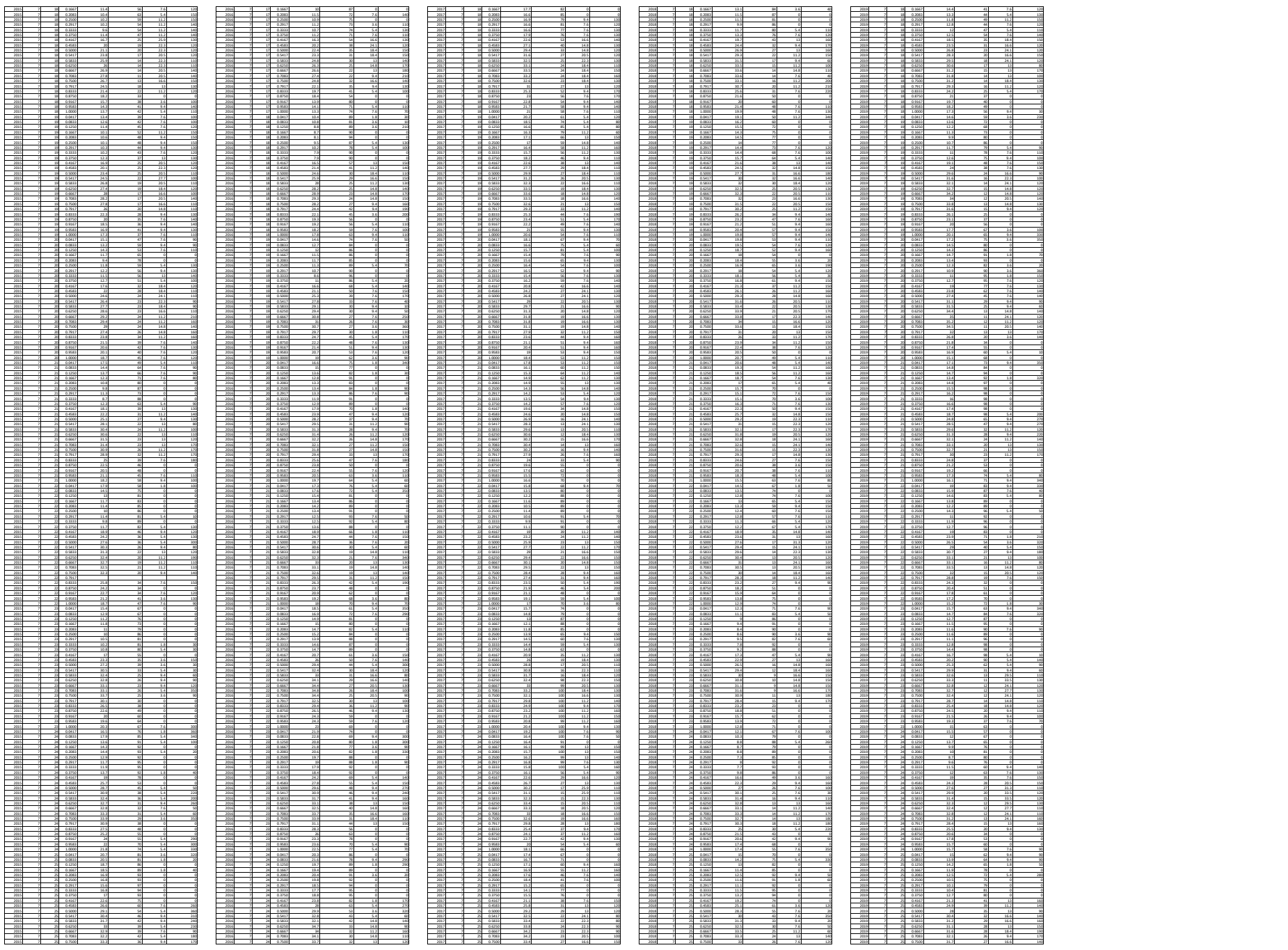

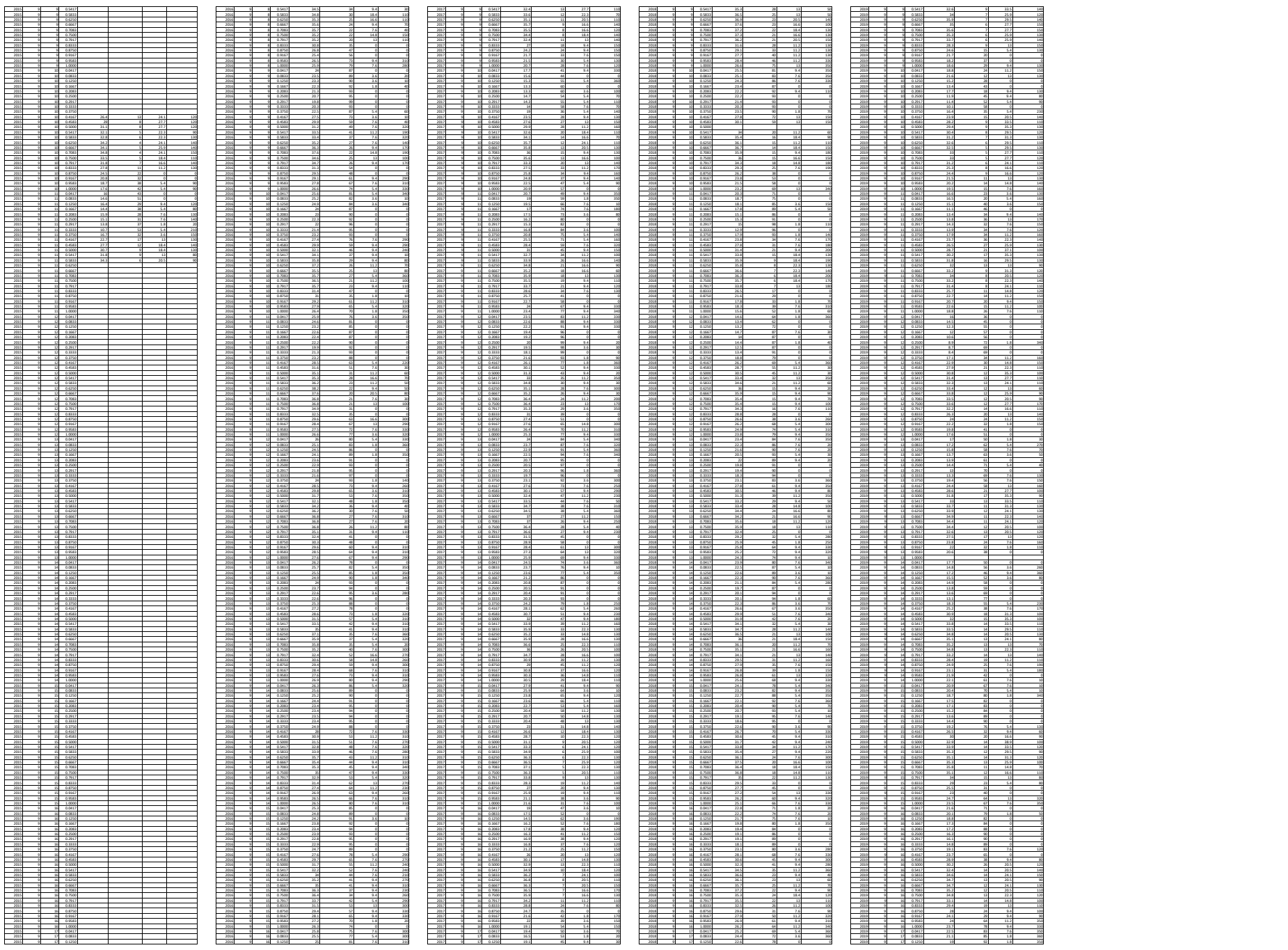

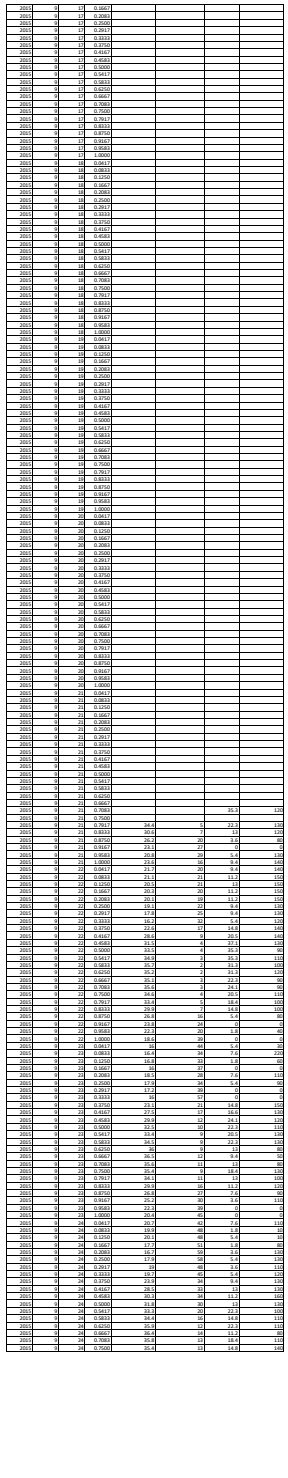
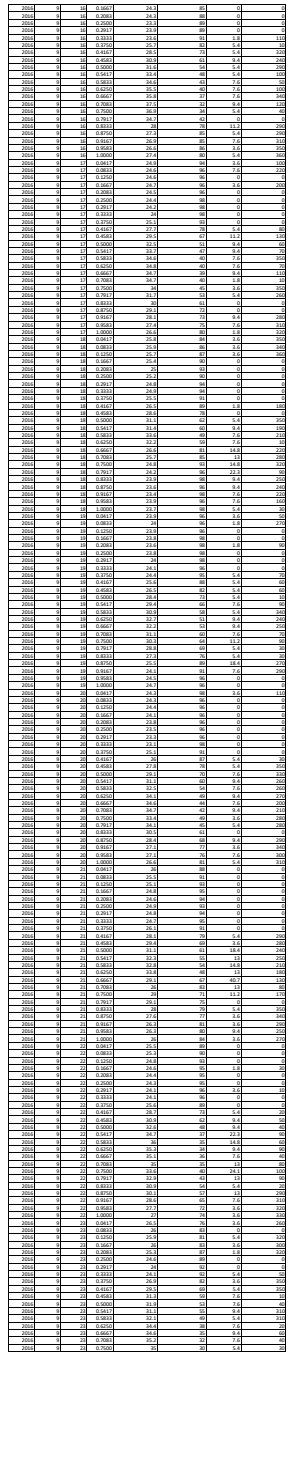
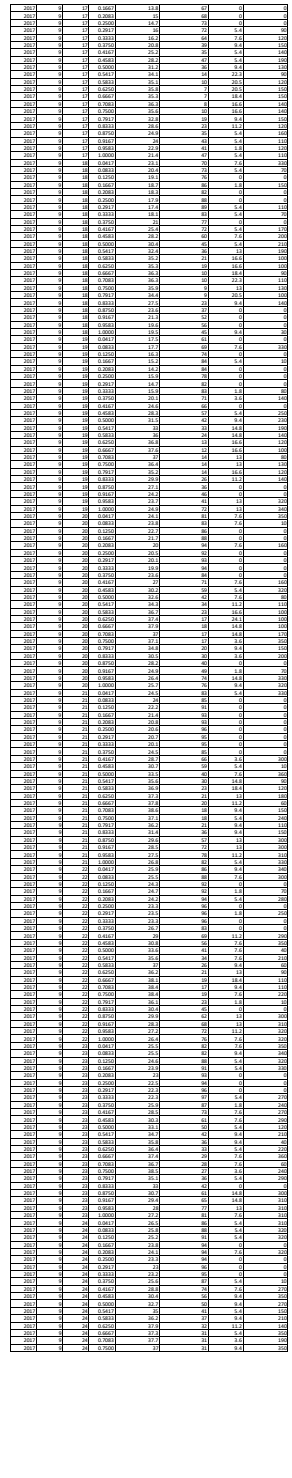
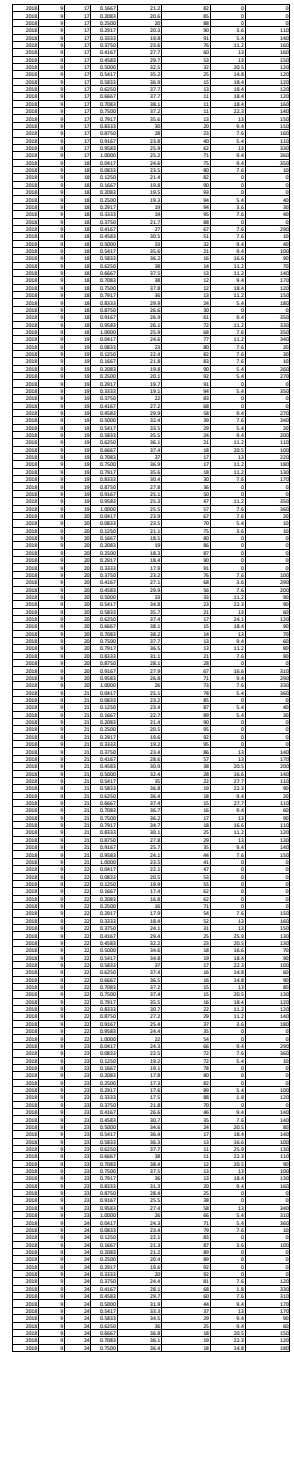
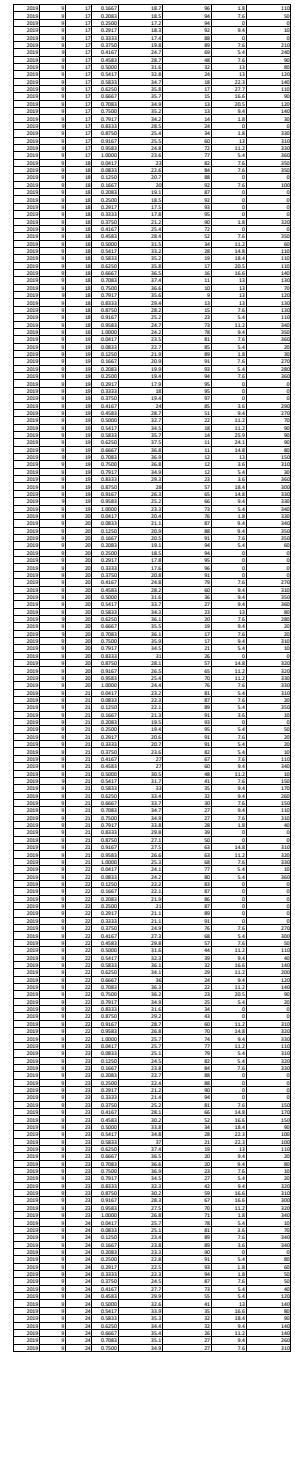

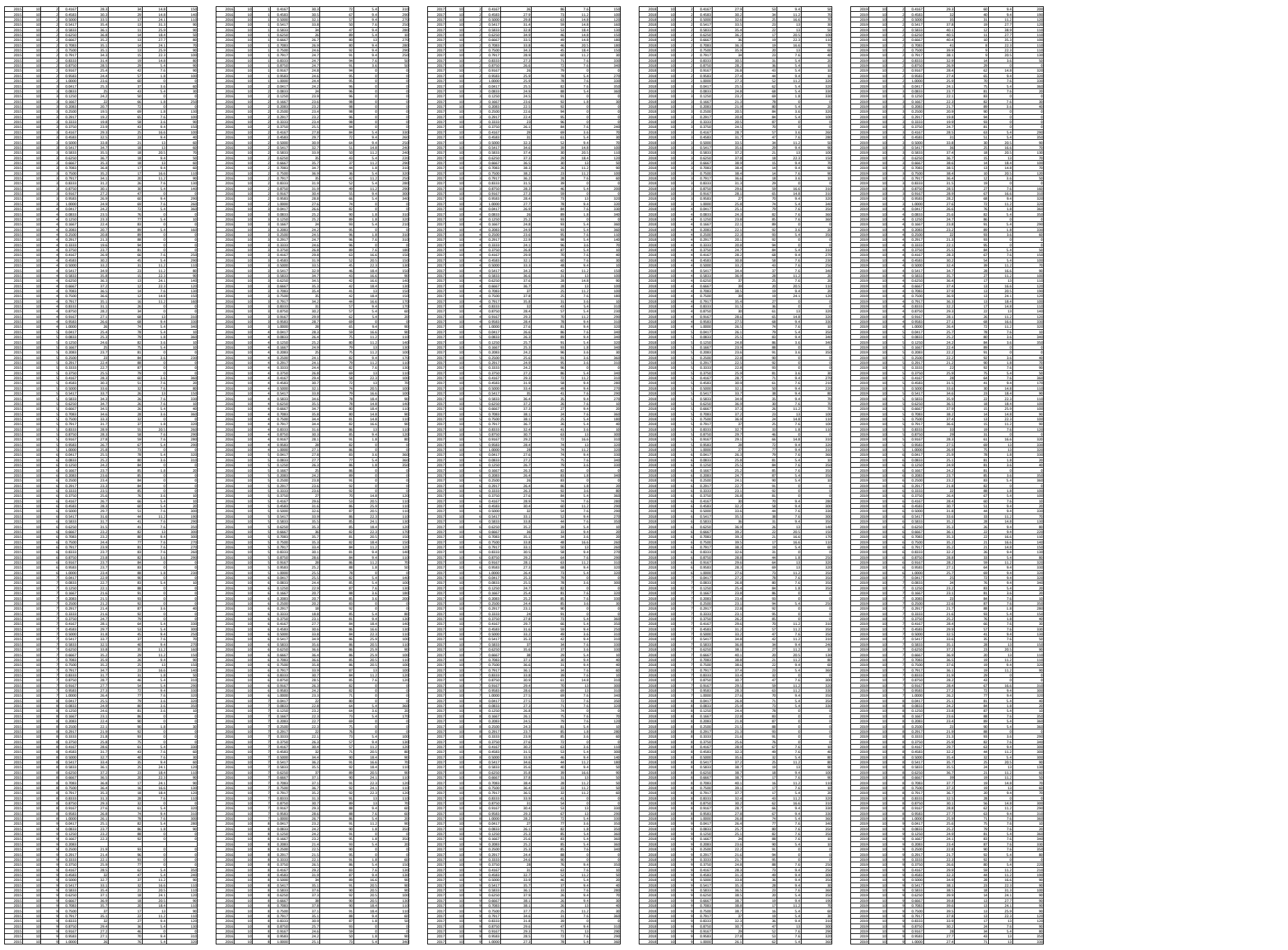

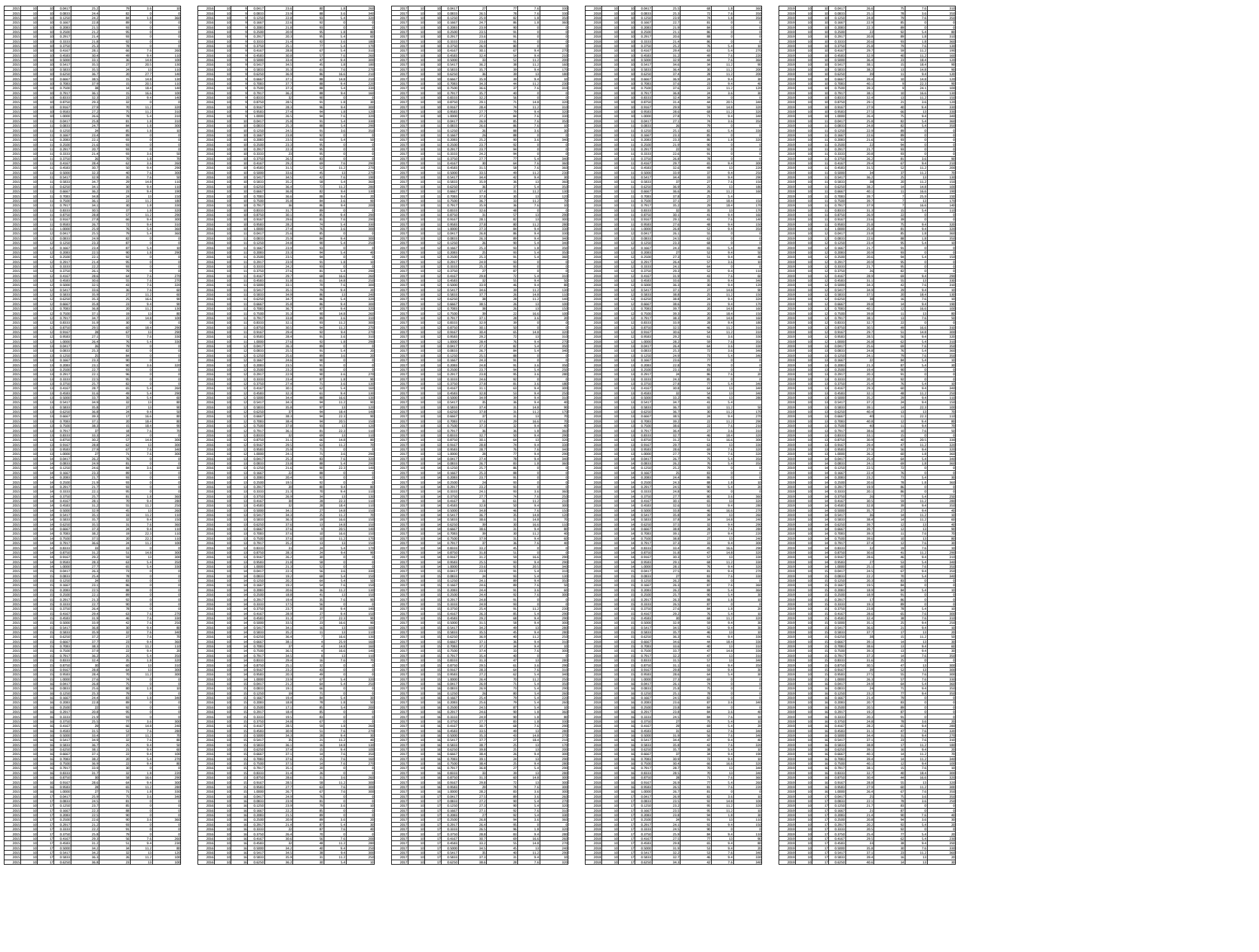

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2015	11	2	0.0833	24.6	96	3.6	290
2015	11	2	0.1250	24.7	96	0	0
2015	11	2	0.1667	24.4	98	0	0
2015	11	2	0.2083	24.3	98	0	0
2015	11	2	0.2500	24.5	96	0	0
2015	11	2	0.2917	24.4	96	0	0
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2015	11	2	0.3750	26.2	92	0	0
2015	11	2	0.4167	28.7	80	7.6	320
2015	11	2	0.4583	30.6	70	5.4	310
2015	11	2	0.5000	32.1	59	11.2	270
2015	11	2	0.5417	33	53	13	250
2015	11	2	0.5833	34.9	44	7.6	300
2015	11	2	0.6250	35.6	42	11.2	270
2015	11	2	0.6667	36.7	36	3.6	340
2015	11	2	0.7083	36.9	34	9.4	290
2015	11	2	0.7500	36.5	36	7.6	240
2015	11	2	0.7917	35	43	5.4	360
2015	11	2	0.8333	32.3	51	3.6	300
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2015	11	2	0.9167	29.5	70	9.4	290
2015	11	2	0.9583	29	71	11.2	310
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2015	11	3	0.0417	24	96	9.4	50
2015	11	3	0.0833	24.5	93	9.4	300
2015	11	3	0.1250	24.7	94	0	0
2015	11	3	0.1667	24.8	95	0	0
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2015	11	3	0.2917	25	98	0	0
2015	11	3	0.3333	25.8	95	0	0
2015	11	3	0.3750	27.7	87	1.8	360
2015	11	3	0.4167	29.8	71	7.6	330
2015	11	3	0.4583	32.2	63	3.6	10
2015	11	3	0.5000	32	60	7.6	280
2015	11	3	0.5417	32.2	57	7.6	290
2015	11	3	0.5833	33.5	52	5.4	150
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2015	11	5	0.7500	36.6	39	3.6	290
2015	11	5	0.7917	31.4	60	13	330
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2015	11	9	0.2500	25.4	89	1.8	330
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2015	11	9	0.3750	28.1	79	5.4	290
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2015	11	9	0.4583	32.3	59	9.4	270
2015	11	9	0.5000	33.9	48	7.6	300

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2016	11	1	0.0833	23.5	96	0	0
2016	11	1	0.1250	23.8	96	1.8	40
2016	11	1	0.1667	23.9	93	0	0
2016	11	1	0.2083	24.2	94	0	0
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2016	11	1	0.2917	24.5	96	0	0
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2016	11	1	0.4167	29.6	84	3.6	30
2016	11	1	0.4583	27.3	82	29.5	170
2016	11	1	0.5000	23.7	98	27.7	130
2016	11	1	0.5417	24.6	95	16.6	130
2016	11	1	0.5833	25.6	91	9.4	220
2016	11	1	0.6250	28.2	75	20.5	180
2016	11	1	0.6667	29.8	64	11.2	190
2016	11	1	0.7083	30.8	58	9.4	230
2016	11	1	0.7500	29.5	67	5.4	300
2016	11	1	0.7917	28.3	79	0	0
2016	11	1	0.8333	27.3	85	0	0
2016	11	1	0.8750	26.5	89	0	0
2016	11	1	0.9167	26	88	5.4	270
2016	11	1	0.9583	25.8	87	7.6	290
2016	11	1	1.0000	25.5	90	1.8	300
2016	11	2	0.0417	24.9	95	0	0
2016	11	2	0.0833	24.8	95	0	0
2016	11	2	0.1250	24.7	96	0	0
2016	11	2	0.1667	24.3	96	0	0
2016	11	2	0.2083	24.2	94	5.4	270
2016	11	2	0.2500	24.2	94	1.8	260
2016	11	2	0.2917	24	95	3.6	220
2016	11	2	0.3333	24.5	93	5.4	200
2016	11	2	0.3750	26.4	83	11.2	140
2016	11	2	0.4167	29.4	65	14.8	100
2016	11	2	0.4583	31.5	57	13	100
2016	11	2	0.5000	33.4	52	7.6	70
2016	11	2	0.5417	34.5	48	9.4	160
2016	11	2	0.5833	35	45	13	150
2016	11	2	0.6250	35.7	43	14.8	160
2016	11	2	0.6667	33.6	43	14.8	170
2016	11	2	0.7083	36.4	36	9.4	170
2016	11	2	0.7500	33.6	49	1.8	350
2016	11	2	0.7917	30.4	64	3.6	330
2016	11	2	0.8333	29.5	66	9.4	290
2016	11	2	0.8750	29	68	1.8	350
2016	11	2	0.9167	27.2	77	9.4	320
2016	11	2	0.9583	26.6	81	0	0
2016	11	2	1.0000	26	84	5.4	290
2016	11	3	0.0417	25.5	87	7.6	260
2016	11	3	0.0833	25.2	88	3.6	260
2016	11	3	0.1250	25.3	87	0	0
2016	11	3	0.1667	24.8	91	0	0
2016	11	3	0.2083	25	93	0	0
2016	11	3	0.2500	24.9	95	0	0
2016	11	3	0.2917	24.5	96	0	0
2016	11	3	0.3333	24.9	95	0	0
2016	11	3	0.3750	26.3	87	0	0
2016	11	3	0.4167	28.6	75	0	0
2016	11	3	0.4583	30.7	61	5.4	330
2016	11	3	0.5000	33	53	1.8	260
2016	11	3	0.5417	35	45	9.4	310
2016	11	3	0.5833	36.5	39	7.6	330
2016	11	3	0.6250	36.7	35	7.6	350
2016	11	3	0.6667	37.7	32	9.4	30
2016	11	3	0.7083	37.8	27	14.8	110
2016	11	3	0.7500	36.4	36	7.6	120
2016	11	3	0.7917	33.4	48	0	0
2016	11	3	0.8333	31.7	52	0	0
2016	11	3	0.8750	30.1	63	0	0
2016	11	3	0.9167	30.5	66	13	310
2016	11	3	0.9583	29.4	71	7.6	310
2016	11	3	1.0000	28.8	75	5.4	360
2016	11	4	0.0417	28.7	72	1.8	10
2016	11	4	0.0833	28.4	78	1.8	340
2016	11	4	0.1250	27.6	83	0	0
2016	11	4	0.1667	27.3	82	0	0
2016	11	4	0.2083	26.6	85	3.6	300
2016	11	4	0.2500	26	89	0	0
2016	11	4	0.2917	25.5	94	0	0
2016	11	4	0.3333	26.4	89	0	0
2016	11	4	0.3750	28.9	80	0	0
2016	11	4	0.4167	30.2	77	9.4	310
2016	11	4	0.4583	32.1	66	5.4	300
2016	11	4	0.5000	33.5	59	1.8	330
2016	11	4	0.5417	34.8	51	7.6	40
2016	11	4	0.5833	35.8	43	9.4	70
2016	11	4	0.6250	37.3	37	5.4	290
2016	11	4	0.6667	38.4	32	11.2	80
2016	11	4	0.7083	38.9	34	3.6	10
2016	11	4	0.7500	38.1	33	0	0
2016	11	4	0.7917	34.5	46	0	0
2016	11	4	0.8333	33	49	11.2	300
2016	11	4	0.8750	31.9	64	14.8	260
2016	11	4	0.9167	30.9	71	11.2	300
2016	11	4	0.9583	29	74	9.4	320
2016	11	4	1.0000	28.3	66	3.6	350
2016	11	5	0.0417	27.9	74	5.4	280
2016	11	5	0.0833	27.3	81	0	0
2016	11	5	0.1250	26.7	84	0	0
2016	11	5	0.1667	26.2	87	0	0
2016	11	5	0.2083	26.2	88	0	0
2016	11	5	0.2500	25.7	91	0	0
2016	11	5	0.2917	25.4	93	0	0
2016	11	5	0.3333	26.1	91	5.4	270
2016	11	5	0.3750	28.8	76	0	0
2016	11	5	0.4167	30.5	74	7.6	290
2016	11	5	0.4583	32.2	66	9.4	250
2016	11	5	0.5000	33.6	60	5.4	230
2016	11	5	0.5417	34.5	54	7.6	240
2016	11	5	0.5833	36.1	48	3.6	80
2016	11	5	0.6250	37.1	42	7.6	250
2016	11	5	0.6667	38.3	38	5.4	340
2016	11	5	0.7083	36.6	41	0	0
2016	11	5	0.7500	32.8	44	9.4	340
2016	11	5	0.7917	29.6	56	13	290
2016	11	5	0.8333	26.6	69	11.2	300
2016	11	5	0.8750	26.5	71	0	0
2016	11	5	0.9167	27	70	5.4	70
2016	11	5	0.9583	27.1	70	0	0
2016	11	5	1.0000	26.3	79	7.6	240
2016	11	6	0.0417	25.9	77	7.6	290
2016	11	6	0.0833	25	84	0	0
2016	11	6	0.1250	24.6	85	0	0
2016	11	6	0.1667	24.6	90	0	0
2016	11	6	0.2083	24.3	91	0	0
2016	11	6	0.2500	24.1	91	5.4	10
2016	11	6	0.2917	24	92	3.6	240
2016	11	6	0.3333	24.7	88	1.8	320
2016	11	6	0.3750	27.6	76	0	0
2016	11	6	0.4167	29.7	74	11.2	270
2016	11	6	0.4583	31.4	64	9.4	250
2016	11	6	0.5000	32.9	59	7.6	280
2016	11	6	0.5417	33.8	53	13	260
2016	11	6	0.5833	34.4	52	11.2	270
2016	11	6	0.6250	34.3	49	9.4	290
2016	11	6	0.6667	34.6	47	9.4	280
2016	11	6	0.7083	35.8	43	7.6	280
2016	11	6	0.7500	34.1	56	7.6	300
2016	11	6	0.7917	29.7	59	14.8	290
2016	11	6	0.8333	28.8	62	5.4	300
2016	11	6	0.8750	27.8	65	5.4	280
2016	11	6	0.9167	26.7	69	3.6	310
2016	11	6	0.9583	25.2	77	5.4	270
2016	11	6	1.0000	25.3	74	5.4	330
2016	11	7	0.0417	24.6	83	1.8	270
2016	11	7	0.0833	24.4	82	0	0
2016	11	7	0.1250	23.2	92	3.6	280
2016	11	7	0.1667	23.4	88	0	0
2016	11	7	0.2083	23.7	86	1.8	360
2016	11	7	0.2500	23.5	92	0	0
2016	11	7	0.2917	23.8	93	0	0
2016	11	7	0.3333	24.6	89	0	0
2016	11	7	0.3750	27.8	84	0	0
2016	11	7	0.4167	30	75	9.4	280
2016	11	7	0.4583	32.1	67	11.2	280
2016	11	7	0.5000	33.2	59	13	270
2016	11	7	0.5417	34.8	48	16.6	270
2016	11	7	0.5833	35.6	46	13	280
2016	11	7	0.6250	37.2	37	11.2	280
2016	11	7	0.6667	37.9	34	9.4	260
2016	11	7	0.7083	38.1	27	11.2	250
2016	11	7	0.7500	35.2	42	7.6	270
2016	11	7	0.7917	32.9	53	14.8	280
2016	11	7	0.8333	29.4	58	14.8	280
2016	11	7	0.8750	28.4	62	7.6	290
2016	11	7	0.9167	27.2	72	1.8	230
2016	11	7	0.9583	27.1	72	0	0
2016	11	7	1.0000	26.5	81	0	0
2016	11	8	0.0417	26.5	87	1.8	330
2016	11	8	0.0833	27.2	90	1.8	320
2016	11	8	0.1250	27	89	3.6	320
2016	11	8	0.1667	26.8	89	0	0
2016	11	8	0.2083	26.4	92	0	0
2016	11	8	0.2500	25.7	94	0	0
2016	11	8	0.2917	25.4	95	0	0
2016	11	8	0.3333	25.7	94	0	0
2016	11	8	0.3750	29	84	1.8	10
2016	11	8	0.4167	30.4	74	11.2	290
2016	11	8	0.4583	32.1	65	13	290
2016	11	8	0.5000	33.3	59	18.4	260

2017	11	1	0.9167	22.2	93	24.1	160
2017	11	1	0.9583	24	85	13	170
2017	11	1	1.0000	23.3	91	11.2	330
2017	11	2	0.0417	23.4	92	11.2	240
2017	11	2	0.0833	23.3	92	5.4	30
2017	11	2	0.1250	23.4	94	3.6	170
2017	11	2	0.1667	22.8	95	0	0
2017	11	2	0.2083	22.5	96	0	0
2017	11	2	0.2500	22	98	0	0
2017	11	2	0.2917	22	98	0	0
2017	11	2	0.3333	22.1	97	1.8	360
2017	11	2	0.3750	24.8	79	5.4	80
2017	11	2	0.4167	27.5	65	9.4	140
2017	11	2	0.4583	29.4	51	13	150
2017	11	2	0.5000	31.5	46	14.8	90
2017	11	2	0.5417	33.9	41	13	90
2017	11	2	0.5833	35.2	29	18.4	90
2017	11	2	0.6250	36.1	18	20.5	140
2017	11	2	0.6667	36.5	14	13	110
2017	11	2	0.7083	36.2	14	9.4	130
2017	11	2	0.7500	36.8	17	1.8	260
2017	11	2	0.7917	34.6	24	9.4	210
2017	11	2	0.8333	29	37	0	0
2017	11	2	0.8750	25.5	67	0	0
2017	11	2	0.9167	23.5	70	5.4	150
2017	11	2	0.9583	22.4	81	0	0
2017	11	2	1.0000	23.5	71	5.4	300
2017	11	3	0.0417	21.9	82	0	0
2017	11	3	0.0833	21	92	0	0
2017	11	3	0.1250	21	91	0	0
2017	11	3	0.1667	20.7	93	0	0
2017	11	3	0.2083	20.4	95	0	0
2017	11	3	0.2500	20	95	5.4	110
2017	11	3	0.2917	20	96	9.4	10
2017	11	3	0.3333	20.4	95	0	0
2017	11	3	0.3750	23.7	89	0	0
2017	11	3	0.4167	26.4	72	1.8	330
2017	11	3	0.4583	30	50	3.6	20
2017	11	3	0.5000	32.6	44	5.4	40
2017	11	3	0.5417	34.4	32	7.6	350
2017	11	3	0.5833	36.3	19	9.4	30
2017	11	3	0.6250	36.9	13	7.6	360
2017	11	3	0.6667	37	12	9.4	90
2017	11	3	0.7083	37.2	13	5.4	330
2017	11	3	0.7500	36.1	21	5.4	350
2017	11	3	0.7917	33.6	33	0	0
2017	11	3	0.8333	28.9	55	0	0
2017	11	3	0.8750	25.8	73	0	0
2017	11	3	0.9167	27.4	71	3.6	300
2017	11	3	0.9583	26.5	77	9.4	340
2017	11	3	1.0000	26.1	83	3.6	300
2017	11	4	0.0417	25	89	0	0
2017	11	4	0.0833	25.1	89	7.6	10
2017	11	4	0.1250	24.4	92	5.4	10
2017	11	4	0.1667	23.5	95	0	0
2017	11	4	0.2083	23.5	96	1.8	120
2017	11	4	0.2500	23.8	94	0	0
2017	11	4	0.2917	23.6	95	5.4	30
2017	11	4	0.3333	24.3	92	0	0
2017	11	4	0.3750	26.7	82	5.4	350
2017	11	4	0.4167	29.6	72	9.4	320
2017	11	4	0.4583	31.1	64	11.2	280
2017	11	4	0.5000	32.9	53	9.4	230
2017	11	4	0.5417	34	48	9.4	240
2017	11	4	0.5833	35.5	45	5.4	210
2017	11	4	0.6250	35.8	39	9.4	170
2017	11	4	0.6667	36.4	35	7.6	170
2017	11	4	0.7083	36.7	29	9.4	30
2017	11	4	0.7500	36.6	30	9.4	40
2017	11	4	0.7917	34.7	39	0	0
2017	11	4	0.8333	31.3	54	11.2	310
2017	11	4	0.8750	29.8	59	13	330
2017	11	4	0.9167	28.4	64	9.4	310
2017	11	4	0.9583	27.5	63	9.4	310
2017	11	4	1.0000	26.7	69	7.6	320
2017	11	5	0.0417	26	75	5.4	340
2017	11	5	0.0833	25.5	80	0	0
2017	11	5	0.1250	25.4	83	5.4	320
2017	11	5	0.1667	25.5	85	1.8	360
2017	11	5	0.2083	25.5	88	3.6	60
2017	11	5	0.2500	24.8	91	0	0
2017	11	5	0.2917	24.6	91	1.8	10
2017	11	5	0.3333	24.9	93	0	0
2017	11	5	0.3750	27.7	80	1.8	40
2017	11	5	0.4167	30.3	69	9.4	270
2017	11	5	0.4583	31.3	61	7.6	270
2017	11	5	0.5000	33.6	47	9.4	50
2017	11	5	0.5417	34.5	43	9.4	340
2017	11	5	0.5833	36.7	36	7.6	50
2017	11	5	0.6250	36.6	33	9.4	360
2017	11	5	0.6667	36.6	32	9.4	360
2017	11	5	0.7083	36.9	30	11.2	70
2017	11	5	0.7500	37	30	7.6	70
2017	11	5	0.7917	35.5	34	5.4	20
2017	11	5	0.8333	32.6	46	0	0
2017	11	5	0.8750	30.8	57	13	310
2017	11	5	0.9167	29.9	59	11.2	310
2017	11	5	0.9583	29.4	64	11.2	280
2017	11	5	1.0000	28.4	70	7.6	310
2017	11	6	0.0417	26.9	76	5.4	350
2017	11	6	0.0833	26.1	79	3.6	350
2017	11	6	0.1250	25.2	86	0	0
2017	11	6	0.1667	25.4	80	5.4	300
2017	11	6	0.2083	24.6	90	1.8	90
2017	11	6	0.2500	24.7	87	0	0
2017	11	6	0.2917	24.5	88	1.8	340
2017	11	6	0.3333	25.5	83	0	0
2017	11	6	0.3750	28.9	68	3.6	320
2017	11	6	0.4167	30.7	64	9.4	280
2017	11	6	0.4583	32.5	56	11.2	300
2017	11	6	0.5000	32.4	55	9.4	310
2017	11	6	0.5417	33.4	50	7.6	20
2017	11	6	0.5833	34.6	46	7.6	20
2017	11	6	0.6250	36.4	38	11.2	280
2017	11	6	0.6667	36.2	37	7.6	320
2017	11	6	0.7083	35.1	40	14.8	220
2017	11	6	0.7500	22.9	89	24.1	320
2017	11	6	0.7917	22.6	87	18.4	330
2017	11	6	0.8333	23.3	93	11.2	70
2017	11	6	0.8750	23.2	95	3.6	30
2017	11	6	0.9167	23.4	96	0	0
2017	11	6	0.9583	23.3	93	9.4	160
2017	11	6	1.0000	23.3	95	5.4	320
2017	11	7	0.0417	23.4	93	9.4	350
2017	11	7	0.0833	23.5	94	5.4	80
2017	11	7	0.1250	23.4	96	5.4	260
2017	11	7	0.1667	23.6	96	0	0
2017	11	7	0.2083	23.2	98	11.2	190
2017	11	7	0.2500	23.5	91	13	210
2017	11	7	0.2917	23.1	96	5.4	50
2017	11	7	0.3333	24	91	9.4	70
2017	11	7	0.3750	26.4	76	16.6	90
2017	11	7	0.4167	27.5	69	14.8	130
2017	11	7	0.4583	28.8	64	11.2	170
2017	11	7	0.5000	29.2	59	7.6	120
2017	11	7	0.5417	31.2	55	7.6	160
2017	11	7	0.5833	33.7	47	7.6	110
2017	11	7	0.6250	34	43	9.4	310
2017	11	7	0.6667	35.5	35	7.6	290
2017	11	7	0.7083	35.9	39	5.4	330
2017	11	7	0.7500	35.5	41	7.6	340
2017	11	7	0.7917	34.3	45	9.4	320
2017	11	7	0.8333	29.4	42	22.3	180
2017	11	7	0.8750	28.3	52	0	0
2017	11	7	0.9167	27.9	58	9.4	250
2017	11	7	0.9583	27.6	64	9.4	270
2017	11	7	1.0000	26.8	72	0	0
2017	11	8	0.0417	26.9	66	7.6	50
2017	11	8	0.0833	26.8	73	11.2	110
2017	11	8	0.1250	26.1	79	5.4	80
2017	11	8	0.1667	25.9	79	5.4	70
2017	11	8	0.2083	25.4	86	5.4	140
2017	11	8	0.2500	25	88	3.6	90
2017	11	8	0.2917	24.8	89	7.6	90
2017	11	8	0.3333	25.3	85	11.2	80
2017	11	8	0.3750	27	77	11.2	130
2017	11	8	0.4167	29.7	57	16.6	90
2017	11	8	0.4583	31.8	48	22.3	110
2017	11	8	0.5000				
2017	11	8	0.5417				
2017	11	8	0.5833				
2017	11	8	0.6250				
2017	11	8	0.6667				
2017	11	8	0.7083				
2017	11	8	0.7500	33.4	47	5.4	320
2017	11	8	0.7917	32.8	50	0	0
2017	11	8	0.8333	31.4	58	5.4	340
2017	11	8	0.8750	29.7	64	7.6	260
2017	11	8	0.9167	28.2	72	1.8	20
2017	11	8	0.9583	30.4	27	20.5	110
2017	11	8	1.0000	27	38	13	170
2017	11	9	0.0417	27.3	32	5.4	180
2017	11	9	0.0833	23.9	58	0	0
2017	11	9	0.1250	21.8	66	0	0
2017	11	9	0.1667	20.9	75	7.6	170
2017	11	9	0.2083	21.3	70	9.4	130
2017	11	9	0.2500	21.3	66	7.6	120
2017	11	9	0.2917	21.9	63	0	0
2017	11	9	0.3333	22.9	61	5.4	100
2017	11	9	0.3750	27.1	35	5.4	110
2017	11	9	0.4167	30	34	9.4	170
2017	11	9	0.4583	31.4	39	11.2	110
2017	11	9	0.5000	33.5	32	7.6	60

2018	11	1	0.9167	30.8	66	13	320
2018	11	1	0.9583	30	69	13	320
2018	11	1	1.0000	29.1	73	7.6	330
2018	11	2	0.0417	28.2	77	5.4	360
2018	11	2	0.0833	27.8	80	5.4	350
2018	11	2	0.1250	27.4	83	1.8	350
2018	11	2	0.1667	26.6	83	3.6	220
2018	11	2	0.2083	26	86	0	0
2018	11	2	0.2500	25.8	89	0	0
2018	11	2	0.2917	25.3	91	0	0
2018	11	2	0.3333	26.1	88	0	0
2018	11	2	0.3750	29.3	72	9.4	360
2018	11	2	0.4167	31	63	7.6	20
2018	11	2	0.4583	32.8	55	7.6	20
2018	11	2	0.5000	36.1	40	11.2	50
2018	11	2	0.5417	38.6	31	13	60
2018	11	2	0.5833	38.7	27	13	70
2018	11	2	0.6250	40.7	24	13	60
2018	11	2	0.6667	41.2	23	9.4	120
2018	11	2	0.7083	39.1	23	11.2	60
2018	11	2	0.7500	36.7	27	31.3	80
2018	11	2	0.7917	34.7	38	7.6	350
2018	11	2	0.8333	32.8	42	1.8	350
2018	11	2	0.8750	31.3	68	16.6	290
2018	11	2	0.9167	30.6	72	9.4	290
2018	11	2	0.9583	29.9	75	9.4	300
2018	11	2	1.0000	29.6	75	7.6	310
2018	11	3	0.0417	28.8	78	7.6	350
2018	11	3	0.0833	28.2	80	0	0
2018	11	3	0.1250	28	81	0	0
2018	11	3	0.1667	27.7	83	7.6	340
2018	11	3	0.2083	27.3	85	0	0
2018	11	3	0.2500	27.2	86	9.4	120
2018	11	3	0.2917	22.9	88	16.6	180
2018	11	3	0.3333	23.1	86	1.8	330
2018	11	3	0.3750	24.4	82	7.6	10
2018	11	3	0.4167	27.3	69	11.2	140
2018	11	3	0.4583	30.2	61	7.6	130
2018	11	3	0.5000	32	57	7.6	350
2018	11	3	0.5417	34.8	49	9.4	340
2018	11	3	0.5833	34.8	47	11.2	280
2018	11	3	0.6250	23.9	88	38.9	170
2018	11	3	0.6667	27.5	84	7.6	290
2018	11	3	0.7083	28.1	72	9.4	180
2018	11	3	0.7500	28	77	5.4	320
2018	11	3	0.7917	26.7	80	11.2	310
2018	11	3	0.8333	25.9	82	5.4	310
2018	11	3	0.8750	25.5	84	7.6	300
2018	11	3	0.9167	25.6	85	7.6	310
2018	11	3	0.9583	25.6	87	13	70
2018	11	3	1.0000	25	88	9.4	350
2018	11	4	0.0417	24.3	90	5.4	300
2018	11	4	0.0833	23.9	88	1.8	350
2018	11	4	0.1250	24.1	91	0	0
2018	11	4	0.1667	23.5	94	3.6	30
2018	11	4	0.2083	23.5	94	0	0
2018	11	4	0.2500	23.5	94	3.6	90
2018	11	4	0.2917	23.3	94	3.6	40
2018	11	4	0.3333	23.6	92	5.4	30
2018	11	4	0.3750	26.6	79	5.4	30
2018	11	4	0.4167	29	67	0	0
2018	11	4	0.4583	31.4	61	7.6	340
2018	11	4	0.5000	33.2	50	9.4	210
2018	11	4	0.5417	34.5	46	9.4	300
2018	11	4	0.5833	35.2	38	5.4	20
2018	11	4	0.6250	35.6	39	5.4	360
2018	11	4	0.6667	36.8	33	11.2	330
2018	11	4	0.7083	36.5	33	7.6	350
2018	11	4	0.7500	35.4	38	1.8	350
2018	11	4	0.7917	34.9	39	9.4	220
2018	11	4	0.8333	31.5	60	16.6	320
2018	11	4	0.8750	27.3	81	9.4	320
2018	11	4	0.9167	27.1	80	9.4	310
2018	11	4	0.9583	26.1	82	5.4	330
2018	11	4	1.0000	25.9	86	0	0
2018	11	5	0.0417	25.8	85	3.6	350
2018	11	5	0.0833	25.4	86	5.4	340
2018	11	5	0.1250	25	87	1.8	320
2018	11	5	0.1667	24.7	89	5.4	340
2018	11	5	0.2083	24.7	88	0	0
2018	11	5	0.2500	24.2	91	0	0
2018	11	5	0.2917	24.3	93	5.4	40
2018	11	5	0.3333	25.4	91	3.6	40
2018	11	5	0.3750	27.8	84	1.8	10
2018	11	5	0.4167	29.7	73	9.4	300
2018	11	5	0.4583	32.2	62	11.2	250
2018	11	5	0.5000	33.7	51	9.4	290
2018	11	5	0.5417	34.8	41	9.4	280
2018	11	5	0.5833	35.7	38	11.2	320
2018	11	5	0.6250	35	39	11.2	320
2018	11	5	0.6667	37.2	33	14.8	270
2018	11	5	0.7083	36.9	32	11.2	250
2018	11	5	0.7500	32.8	48	9.4	350
2018	11	5	0.7917	32.4	57	11.2	270
2018	11	5	0.8333	30.5	66	11.2	260
2018	11	5	0.8750	30.3	65	7.6	320
2018	11	5	0.9167	28.5	67	13	340
2018	11	5	0.9583	27.6	71	9.4	320
2018	11	5	1.0000	27	75	5.4	10
2018	11	6	0.0417	26.1	79	5.4	30
2018	11	6	0.0833	25.4	83	5.4	50
2018	11	6	0.1250	24.9	86	5.4	50
2018	11	6	0.1667	25	89	5.4	50
2018	11	6	0.2083	24.9	90	1.8	60
2018	11	6	0.2500	24.9	91	0	0
2018	11	6	0.2917	24.6	92	0	0
2018	11	6	0.3333	25.1	90	0	0
2018	11	6	0.3750	27.6	82	1.8	10
2018	11	6	0.4167	30	69	7.6	310
2018	11	6	0.4583	32.2	59	9.4	290
2018	11	6	0.5000	33.7	49	9.4	290
2018	11	6	0.5417	34.9	46	9.4	260
2018	11	6	0.5833	36.8	38	5.4	230
2018	11	6	0.6250	36.5	35	5.4	310
2018	11	6	0.6667	37.8	33	5.4	20
2018	11	6	0.7083	28.2	72	14.8	30
2018	11	6	0.7500	34.2	52	7.6	330
2018	11	6	0.7917	33.4	47	7.6	350
2018	11	6	0.8333	30.3	63	20.5	330
2018	11	6	0.8750	28.5	72	14.8	310
2018	11	6	0.9167	27.8	75	7.6	300
2018	11	6	0.9583	27.2	78	5.4	320
2018	11	6	1.0000	26.6	79	0	0
2018	11	7	0.0417	26.7	79	5.4	330
2018	11	7	0.0833	26.3	83	0	0
2018	11	7	0.1250	26.1	84	0	0
2018	11	7	0.1667	25.6	88	0	0
2018	11	7	0.2083	25.2	90	5.4	50
2018	11	7	0.2500	25.5	90	5.4	30
2018	11	7	0.2917	25.8	89	5.4	30
2018	11	7	0.3333	26.5	86	0	0
2018	11	7	0.3750	28.9	72	5.4	20
2018	11	7	0.4167	31.2	62	9.4	10
2018	11	7	0.4583	33.5	52	7.6	330
2018	11	7	0.5000	34.3	44	9.4	310
2018	11	7	0.5417	36.1	39	9.4	200
2018	11	7	0.5833	36.6	36	7.6	340
2018	11	7	0.6250	36.4	34	5.4	200
2018	11	7	0.6667	38.2	30	11.2	270
2018	11	7	0.7083	37.9	32	5.4	190
2018	11	7	0.7500	35.6	38	3.6	360
2018	11	7	0.7917	33.6	45	18.4	250
2018	11	7	0.8333	29.7	66	13	300
2018	11	7	0.8750	28.8	68	9.4	280
2018	11	7	0.9167	28.4	75	7.6	320
2018	11	7	0.9583	28.4	75	7.6	330
2018	11	7	1.0000	28.1	79	9.4	340
2018	11	8	0.0417	27.8	81	7.6	330
2018	11	8	0.0833	27.6	84	7.6	350
2018	11	8	0.1250	27.1	86	3.6	360
2018	11	8	0.1667	26.5	88	0	0
2018	11	8	0.2083	25.9	90	0	0
2018	11	8	0.2500	25.6	90	1.8	90
2018	11	8	0.2917	25.1	92	0	0
2018	11	8	0.3333	26	90	0	0
2018	11	8	0.3750	28.5	79	5.4	250
2018	11	8	0.4167	30.1	71	9.4	290
2018	11	8	0.4583	31.8	62	13	280
2018	11	8	0.5000	32.8	54	5.4	310
2018	11	8	0.5417	35	45	5.4	310
2018	11	8	0.5833	36.1	41	11.2	240
2018	11	8	0.6250	36.8	36	13	180
2018	11	8	0.6667	37.4	33	7.6	360
2018	11	8	0.7083	38.9	31	7.6	230
2018	11	8	0.7500	37.7	30	5.4	100
2018	11	8	0.7917	36.8	33	11.2	230
2018	11	8	0.8333	27.6	76	7.6	150
2018	11	8	0.8750	28.4	69	13	270
2018	11	8	0.9167	27.8	67	7.6	290
2018	11	8	0.9583	27.6	69	0	0
2018	11	8	1.0000	27.6	74	0	0
2018	11	9	0.0417	26.6	81	3.6	50
2018	11	9	0.0833	26.7	84	0	0
2018	11	9	0.1250	26.3	86	3.6	350
2018	11	9	0.1667	26.5	83	1.8	340
2018	11	9	0.2083	25.7	88	0	0
2018	11	9	0.2500	25.1	87	0	0
2018	11	9	0.2917	24.9	88	0	0
2018	11	9	0.3333	26.2	84	0	0
2018	11	9	0.3750	28.3	73	3.6	10
2018	11	9	0.4167	30.4	66	9.4	330
2018	11	9	0.4583	32.6	56	1.8	320
2018	11	9	0.5000	34.5	51	7.6	190

2019	11	1	0.9167	27.6	60	7.6	340
2019	11	1	0.9583	26.5	67	7.6	350
2019	11	1	1.0000	25.6	71	1.8	320
2019	11	2	0.0417	25.3	75	7.6	280
2019	11	2	0.0833	25.3	76	5.4	300
2019	11	2	0.1250	23.8	82	1.8	40
2019	11	2	0.1667	23.8	82	3.6	20
2019	11	2	0.2083	23.7	82	1.8	30
2019	11	2	0.2500	23.3	86	5.4	50
2019	11	2	0.2917	23.2	88	0	0
2019	11	2	0.3333	24.6	86	0	0
2019	11	2	0.3750	27.8	76	7.6	20
2019	11	2	0.4167	30.2	67	11.2	330
2019	11	2	0.4583	31.6	57	13	340
2019	11	2	0.5000	32.8	47	13	330
2019	11	2	0.5417	34.4	41	16.6	340
2019	11	2	0.5833	35.2	39	16.6	320
2019	11	2	0.6250	35.2	33	11.2	320
2019	11	2	0.6667	36.1	31	13	340
2019	11	2	0.7083	33.3	37	27.7	260
2019	11	2	0.7500	35.2	33	16.6	260
2019	11	2	0.7917	34.4	32	16.6	280
2019	11	2	0.8333	32	44	11.2	330
2019	11	2	0.8750	29.1	59	9.4	360
2019	11	2	0.9167	28.3	64	5.4	20
2019	11	2	0.9583	28.7	64	5.4	350
2019	11	2	1.0000	28.2	66	5.4	10
2019	11	3	0.0417	27.4	69	0	0
2019	11	3	0.0833	26.9	73	7.6	340
2019	11	3	0.1250	25.9	77	0	0
2019	11	3	0.1667	25.6	85	5.4	340
2019	11	3	0.2083	25.4	85	0	0
2019	11	3	0.2500	25.7	86	3.6	350
2019	11	3	0.2917	25.4	87	0	0
2019	11	3	0.3333	26.2	84	0	0
2019	11	3	0.3750	28.7	75	9.4	330
2019	11	3	0.4167	30.6	59	14.8	340
2019	11	3	0.4583	32.5	51	13	310
2019	11	3	0.5000	33.2	46	11.2	310
2019	11	3	0.5417	35.4	37	11.2	330
2019	11	3	0.5833	37.5	33	13	320
2019	11	3	0.6250	36.6	32	18.4	290
2019	11	3	0.6667	34	43	14.8	360
2019	11	3	0.7083	33.6	45	14.8	330
2019	11	3	0.7500	33.7	39	13	310
2019	11	3	0.7917	33.3	37	9.4	320
2019	11	3	0.8333	32.2	43	9.4	330
2019	11	3	0.8750	30.1	54	11.2	340
2019	11	3	0.9167	28.8	59	9.4	330
2019	11	3	0.9583	28.4	62	7.6	350
2019	11	3	1.0000	27.8	66	5.4	330
2019	11	4	0.0417	26.8	75	0	0
2019	11	4	0.0833	26.5	80	5.4	10
2019	11	4	0.1250	26.6	82	5.4	340
2019	11	4	0.1667	25.9	83	0	0
2019	11	4	0.2083	25.8	83	7.6	20
2019	11	4	0.2500	25.9	83	0	0
2019	11	4	0.2917	25.5	87	5.4	20
2019	11	4	0.3333	26.3	85	0	0
2019	11	4	0.3750	28.4	75	7.6	10
2019	11	4	0.4167	29.9	65	13	360
2019	11	4	0.4583	32	52	11.2	360
2019	11	4	0.5000	33.5	43	11.2	360
2019	11	4	0.5417	35.1	41	13	360
2019	11	4	0.5833	36.8	34	7.6	340
2019	11	4	0.6250	36.3	33	9.4	330
2019	11	4	0.6667	35.8	33	11.2	350
2019	11	4	0.7083	36.5	40	24.1	250
2019	11	4	0.7500	36.3	36	14.8	250
2019	11	4	0.7917	35.3	39	13	260
2019	11	4	0.8333	30.4	57	11.2	350
2019	11	4	0.8750	28.5	68	3.6	350
2019	11	4	0.9167	27.3	77	5.4	350
2019	11	4	0.9583	26.2	87	9.4	180
2019	11	4	1.0000	26.1	84	5.4	330
2019	11	5	0.0417	25.5	85	7.6	290
2019	11	5	0.0833	25.3	89	7.6	120
2019	11	5	0.1250	25.3	88	1.8	230
2019	11	5	0.1667	25.1	90	0	0
2019	11	5	0.2083	25	92	9.4	140
2019	11	5	0.2500	24.3	93	1.8	190
2019	11	5	0.2917	24.2	94	7.6	350
2019	11	5	0.3333	24.5	94	3.6	260
2019	11	5	0.3750	25.8	86	9.4	260
2019	11	5	0.4167	26.9	85	5.4	310
2019	11	5	0.4583	28.3	69	13	130
2019	11	5	0.5000	28.9	67	13	100
2019	11	5	0.5417	30	60	9.4	90
2019	11	5	0.5833	30.7	58	9.4	200
2019	11	5	0.6250	32.6	49	13	150
2019	11	5	0.6667	34.2	42	13	150
2019	11	5	0.7083	34.2	45	18.4	200
2019	11	5	0.7500	31.4	53	11.2	360
2019	11	5	0.7917	25.5	82	37.1	110
2019	11	5	0.8333	24	88	13	270
2019	11	5	0.8750	24.5	88	14.8	250
2019	11	5	0.9167	24.3	87	5.4	300
2019	11	5	0.9583	24.2	88	1.8	50
2019	11	5	1.0000	24.8	86	1.8	40
2019	11	6	0.0417	24.6	88	0	0
2019	11	6	0.0833	24.6	89	0	0
2019	11	6	0.1250	24.6	87	5.4	10
2019	11	6	0.1667	24.4	89	0	0
2019	11	6	0.2083	24.6	90	0	0
2019	11	6	0.2500	24.5	91	0	0
2019	11	6	0.2917	24.3	91	1.8	100
2019	11	6	0.3333	24.7	92	1.8	140
2019	11	6	0.3750	27.1	80	7.6	150
2019	11	6	0.4167	29.1	70	7.6	190
2019	11	6	0.4583	30.8	60	9.4	160
2019	11	6	0.5000	34	54	14.8	200
2019	11	6	0.5417	36.2	32	22.3	140
2019	11	6	0.5833	35.9	32	13	110
2019	11	6	0.6250	37.9	26	20.5	150
2019	11	6	0.6667	37.9	25	11.2	120
2019	11	6	0.7083	38.7	23	22.3	130
2019	11	6	0.7500	38.7	22	14.8	160
2019	11	6	0.7917	37.7	22	18.4	130
2019	11	6	0.8333	34.2	28	9.4	140
2019	11	6	0.8750	30.7	43	0	0
2019	11	6	0.9167	28.6	50	0	0
2019	11	6	0.9583	26.8	66	0	0
2019	11	6	1.0000	25.5	70	0	0
2019	11	7	0.0417	24.5	78	0	0
2019	11	7	0.0833	26	80	3.6	350
2019	11	7	0.1250	26.5	80	5.4	30
2019	11	7	0.1667	26.8	85	7.6	10
2019	11	7	0.2083	26.7	85	7.6	30
2019	11	7	0.2500	26.1	88	7.6	20
2019	11	7	0.2917	25.5	90	1.8	360
2019	11	7	0.3333	26.2	90	5.4	230
2019	11	7	0.3750	28.5	77	3.6	350
2019	11	7	0.4167	30.9	66	5.4	360
2019	11	7	0.4583	32.6	55	5.4	330
2019	11	7	0.5000	35.3	35	9.4	30
2019	11	7	0.5417	36.3	32	13	10
2019	11	7	0.5833	36.4	27	11.2	60
2019	11	7	0.6250	37.5	24	7.6	60
2019	11	7	0.6667	38	22	13	90
2019	11	7	0.7083	37	22	5.4	60
2019	11	7	0.7500	38.5	21	13	270
2019	11	7	0.7917	35	40	18.4	310
2019	11	7	0.8333	31.5	59	16.6	280
2019	11	7	0.8750	29.8	70	11.2	290
2019	11	7	0.9167	28.7	74	11.2	280
2019	11	7	0.9583	27.8	77	7.6	290
2019	11	7	1.0000	26.6	82	3.6	340
2019	11	8	0.0417	25.9	86	7.6	20
2019	11	8	0.0833	25.8	88	0	0
2019	11	8	0.1250	24.9	90	0	0
2019	11	8	0.1667	25.4	90	7.6	10
2019	11	8	0.2083	25.5	91	5.4	360
2019	11	8	0.2500	24.7	90	0	0
2019	11	8	0.2917	24.2	92	0	0
2019	11	8	0.3333	25.1	91	0	0
2019	11	8	0.3750	28.6	72	1.8	320
2019	11	8	0.4167	31	60	9.4	340
2019	11	8	0.4583	32.8	48	9.4	300
2019	11	8	0.5000	34.1	40	9.4	300
2019	11	8	0.5417	35.6	36	11.2	270
2019	11	8	0.5833	36.9	32	7.6	100
2019	11	8	0.6250	37.8	29	11.2	70
2019	11	8	0.6667	37.4	29	11.2	80
2019	11	8	0.7083	36.7	29	1.8	30
2019	11	8	0.7500	36	32	5.4	350
2019	11	8	0.7917	32	54	14.8	320
2019	11	8	0.8333	30.4	60	13	300
2019	11	8	0.8750	29.4	66	14.8	310
2019	11	8	0.9167	28.4	69	9.4	320
2019	11	8	0.9583	27.5	71	7.6	340
2019	11	8	1.0000	26.7	75	7.6	350
2019	11	9	0.0417	25.8	79	3.6	30
2019	11	9	0.0833	25.5	83	5.4	360
2019	11	9	0.1250	25.1	85	1.8	30
2019	11	9	0.1667	25.5	81	9.4	10
2019	11	9	0.2083	24.5	84	0	0
2019	11	9	0.2500	24.1	88	0	0
2019	11	9	0.2917	23.9	89	7.6	50
2019	11	9	0.3333	25.5	84	5.4	40
2019	11	9	0.3750	28.7	73	3.6	300
2019	11	9	0.4167	30.6	63	7.6	330
2019	11	9	0.4583	32.8	51	9.4	310
2019	11	9	0.5000	34.8	46	11.2	340

2010	12	31	0.8750	27.9	83	11.2	305
2010	12	31	0.9167	27.2	90	7.6	290
2010	12	31	0.9583	27.1	89	9.4	291
2011	1	31	1.0000	23.1	96	18.4	205